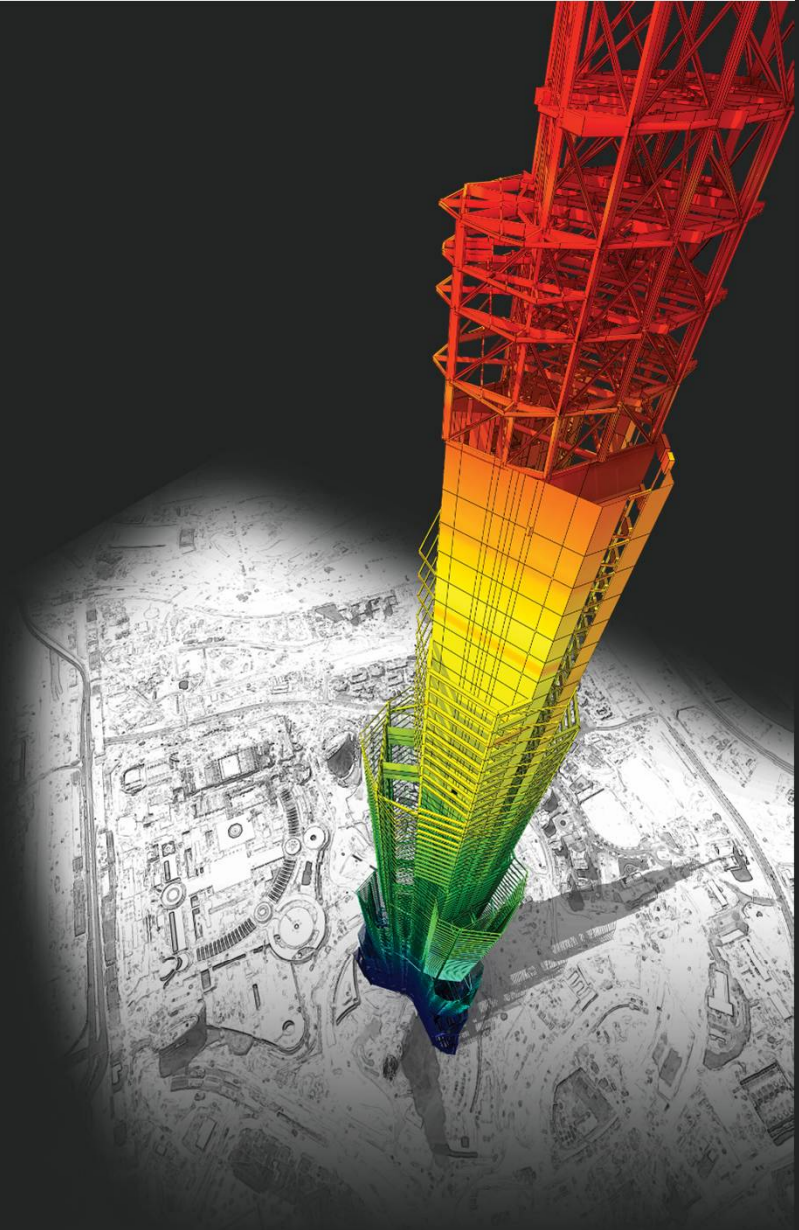


# Release Note

Release Date : Nov. 2024.

Product Ver. : midas Gen 2024 (v1.1)



*DESIGN OF General Structures*

*Integrated Design System for Building and General Structures*

# Index

- **midas Gen**

**Improved Steel Design as per EC3 : 2005**

1. *Seismic Design as per EC8-1 : 2004*
2. *Improvement of “Check Interaction of Combined Resistance”*
3. *Add Interaction factor( $k_{ij}$ ) as per Annex B*
4. *Calculation of  $M_{cr}$  considering one-way symmetrical section and load position*

**Wind loads**

1. *Added Wind loads as per ASCE7-16 & ASCE7-22*

**Wind Pressure**

1. *Added Area/Beam/Nodal Wind Pressure in Wind Pressure feature*
2. *Beam Wind Pressure*
3. *Area Wind Pressure*
4. *Nodal Wind Pressure*
5. *Velocity Pressure*
6. *Improvement of Wind Pressure function*

**Rebar Detail Table**

1. *Support the Rebar detail table according to design provisions*

**Convenience function added**

1. *Angle information in Query Dialog*
2. *Objects selection by load information*
3. *Improvement of Elastic & General Link Table*

↓ Go to **FREE TRIAL**

↓ **INSTALLER DOWNLOAD**

### ***Irregularity Check according to NTC 2022 [NTC-DCEC (2017)]***

1. *Torsional Irregularity & Weight Irregularity*
2. *Stiffness Irregularity*
3. *Capacity Irregularity*

### ***Gen-Revit 2024 Linker***

#### ***Interface for Gen - IDEA Statica Connection***

#### ***Added New Sections***

#### ***ETC.***

1. *Application of “fs” calculated by service load combinations*
2. *Improvement of Cyclic Shear Resistance table*
3. *Generation of Column Fiber Model*

## **• Design +**

### ***Add Design as per ACI318(M)-19***

### ***Improvement on Combined Footing as per ACI318-14 and upper version***

### ***Batch Beam & Column Design***

[↓ Go to FREE TRIAL](#)[↓ INSTALLER DOWNLOAD](#)

*midas* **Gen**

# Improved Steel Design as per EC3 : 2005

## 1. Seismic Design as per EC8-1 : 2004 (Continuous)

**Steel Design Code** ✕

Design Code : Eurocode3:05 ▼

National Annex : Recommended ▼

All Beams/Girders are Laterally Braced

Check Beam/Column Deflection

Apply Special Provisions for Seismic Design

Behaviour and Overstrength Factors

q = 2 γ<sub>ov</sub> = 1,25

Steel Frame Type: Moment frames ▼

Non-seismic Member: None ▼ ...

Biaxial moments for buckling resistance

Biaxial moments at the same location

Maximum moments along the member

Consider as linear summation for class 1,2 (Eq.6.2)

Method for interaction factor, kij

By Code  Annex A  Annex B

Point of load application for M<sub>cr</sub>

Top  Shear Center  Bottom

- Check “Ductility Class” γ according to Table 6.3

→ Evaluate the ductility class of the section required by the seismic provisions according to the inputted behavior factor(q)

**Table 6.3: Requirements on cross-sectional class of dissipative elements depending on Ductility Class and reference behaviour factor**

| Ductility class | Reference value of behaviour factor q | Required cross-sectional class |
|-----------------|---------------------------------------|--------------------------------|
| DCM             | 1,5 < q ≤ 2                           | class 1, 2 or 3                |
|                 | 2 < q ≤ 4                             | class 1 or 2                   |
| DCH             | q > 4                                 | class 1                        |

```

[[[*]] CHECK CROSS-SECTIONAL CLASS FOR SEISMIC DESIGN.
( ). Check cross-sectional class.
[ EN 1998-1:2004 6.5.3 Table 6.3 ]
-. q = 4,000 (Behaviour factor; User Defined Value)
-. 2 < q ≤ 4
  Ductility class = DCM
  Required cross-sectional class = Class 1 or 2
-. Class 4 > Class 1 or 2 ----> NOT ACCEPTABLE !
  Increase section dimensions. (Failure)
        
```

- Column’s Seismic Design under “Moment Frame” system

### 1. Calculation of member design forces

$$N_{Ed} = N_{Ed,G} + 1,1\gamma_{ov} \Omega N_{Ed,E} \qquad \Omega_i = M_{pl,Rd,i}/M_{Ed,i} \quad : \text{Apply Min. } \Omega \text{ at all Joint beams}$$

$$M_{Ed} = M_{Ed,G} + 1,1\gamma_{ov} \Omega M_{Ed,E} \qquad \gamma_{ov} = 1,25 \quad : \text{Apply input value in dialog box}$$

$$V_{Ed} = V_{Ed,G} + 1,1\gamma_{ov} \Omega V_{Ed,E}$$

### 2. Shear design

$$\frac{V_{Ed}}{V_{pl,Rd}} \leq 0,5$$

# Improved Steel Design as per EC3 : 2005

## 1. Seismic Design as per EC8-1 : 2004 (Continuous)

**Steel Design Code** ✕

Design Code : Eurocode3:05 ▼

National Annex : Recommended ▼

All Beams/Girders are Laterally Braced

Check Beam/Column Deflection

Apply Special Provisions for Seismic Design

Behaviour and Overstrength Factors

q = 2      γ<sub>ov</sub> = 1,25

Steel Frame Type Moment frames ▼

Non-seismic Member None ▼ ...

Biaxial moments for buckling resistance

Biaxial moments at the same location

Maximum moments along the member

Consider as linear summation for class 1,2 (Eq.6.2)

Method for interaction factor, kij

By Code     Annex A     Annex B

Point of load application for M<sub>cr</sub>

Top     Shear Center     Bottom

OK
Close

- Beam Design under "Moment Frame" system  
→ Check the conditions on the right for the beam end.

$$\frac{M_{Ed}}{M_{pl,Rd}} \leq 1,0$$

$$\frac{N_{Ed}}{N_{pl,Rd}} \leq 0,15$$

$$\frac{V_{Ed}}{V_{pl,Rd}} \leq 0,5 \qquad V_{Ed} = V_{Ed,G} + V_{Ed,M}$$

$$\qquad \qquad \qquad V_{Ed,M} = (M_{pl,Rd,A} + M_{pl,Rd,B})/L$$

(3) For sections belonging to cross-sectional class 3, expressions (6.2) to (6.5) should be checked replacing  $N_{pl,Rd}$ ,  $M_{pl,Rd}$ ,  $V_{pl,Rd}$  with  $N_{cl,Rd}$ ,  $M_{cl,Rd}$ ,  $V_{cl,Rd}$ .

- Ductility Design (Strong column – Weak beam) under "Moment Frame" system  
→ Check "Steel Strong Column-Weak Beam Ratio" in Table result.  
→ Steel Design > Steel Strong Column-Weak Beam Ratio > Steel Strong Column-Weak Beam Ratio Table

| Node   | Column Local Axis | LCB   | Column Strength (kN-m) | Beam Strength (kN-m) | Ratio | Remark |
|--|-------------------|-------|------------------------|----------------------|-------|--------|
| Acceptance Limit for SCWB C/B Flexural Capacity Ratio: 1.3             |                   |       |                        |                      |       |        |
| Input Acceptance Limit Value and Press 'Apply' button to change value. |                   |       |                        |                      | 1.30  | Apply  |
| 2  | Local y           | sLCB2 | 1469.1003              | 623.0279             | 2.36  | OK     |
| 2  | Local z           | sLCB2 | 2884.1233              | 2264.1604            | 1.27  | N/A    |
| 3  | Local y           | sLCB2 | 1469.1003              | 0.0000               | 99.99 | -      |
| 3  | Local z           | sLCB2 | 2884.1233              | 1703.4353            | 1.69  | OK     |
| 4  | Local y           | sLCB2 | 1469.1003              | 0.0000               | 99.99 | -      |
| 4  | Local z           | sLCB2 | 2884.1233              | 1703.4353            | 1.69  | OK     |
| 5  | Local y           | sLCB2 | 0.0000                 | 623.0279             | 0.00  | CHK    |

## Improved Steel Design as per EC3 : 2005

### 1. Seismic Design as per EC8-1 : 2004 (Continuous)

Steel Design Code

Design Code : Eurocode3:05

National Annex : Recommended

All Beams/Girders are Laterally Braced

Check Beam/Column Deflection

Apply Special Provisions for Seismic Design

Behaviour and Overstrength Factors

q = 2       $\gamma_{ov} = 1,25$

Steel Frame Type: Braced frames

Non-seismic Member: None

Biaxial moments for buckling resistance

Biaxial moments at the same location

Maximum moments along the member

Consider as linear summation for class 1,2 (Eq. 6.2)

Method for interaction factor,  $k_{ij}$

By Code     Annex A     Annex B

Point of load application for  $M_{cr}$

Top     Shear Center     Bottom

OK    Close

- Beam & Column Design under "Braced Frame"
  - Design to have Min. resistance for an axial force by reviewing according to Equation 6.12 below.
  - Only the concentrated braced frame type is supported.

(1) Beams and columns with axial forces should meet the following minimum resistance requirement:

$$N_{pl,Rd}(M_{Ed}) \geq N_{Ed,G} + 1.1 \gamma_{ov} \Omega N_{Ed,E} \quad (6.12)$$

$$N_{pl,Rd} = A_f y / \gamma_{M0} \text{ (Class 1\&2\&3)}$$

- Non-seismic member
  - Groups that do not apply a seismic design can be set.

## Improved Steel Design as per EC3 : 2005

### 2. Improvement of "Check Interaction of Combined Resistance"

**Steel Design Code** ✕

Design Code : Eurocode3:05 ▼

National Annex : Recommended ▼

All Beams/Girders are Laterally Braced

Check Beam/Column Deflection

Apply Special Provisions for Seismic Design

Biaxial moments for buckling resistance

Biaxial moments at the same location

Maximum moments along the member

Consider as linear summation for class 1,2 (Eq. 6.2)

Method for interaction factor,  $k_{ij}$

By Code  Annex A  Annex B

Point of load application for  $M_{cr}$

Top  Shear Center  Bottom

OK Close

Until the previous version, the combination ratio based on the EC3:05 was checked by using Max (Rmax1, Rmax2). But, "Rmax1" is just a 'conservative approach' and basically checking by "Rmax2" can get more precise results. Therefore, the options to control the design as shown below was added.

When checking Interaction Ratio of Bending & Axial force

1. Check on : apply Max(Rmax1,Rmax2) (the same method as the previous version)
2. Check off : apply only Rmax2 (Default method)

In case considering "Lateral & Lateral-torsion"

1. Check on :  $R_{max} = \text{Max}[(R_{max1}, R_{max2}), \text{Max}(R_{max\_LT1}, R_{max\_LT2})]$  (the same method as the previous version)
2. Check off :  $R_{max} = \text{Max}[R_{max2}, \text{Max}(R_{max\_LT1}, R_{max\_LT2})]$  (Default method)

**Rmax1 : EC3:05 6.2.9 (Eq. 6.31~6.41)**

$$\left[ \frac{M_{y,Ed}}{M_{N,y,Rd}} \right]^{\alpha} + \left[ \frac{M_{z,Ed}}{M_{N,z,Rd}} \right]^{\beta} \leq 1 \quad \text{for Class 1\&2 sections}$$

I and H section:  $\alpha=2$ ;  $\beta=5n$  but  $\beta \geq 1$

**Rmax2 : EC3:05 6.2.1.(Eq. 6,2)**

$$\frac{N_{Ed}}{N_{Rd}} + \frac{M_{y,Ed}}{M_{y,Rd}} + \frac{M_{z,Ed}}{M_{z,Rd}} \leq 1 \quad \text{for Class 1,2,3 \& 4 sections}$$



# Improved Steel Design as per EC3 : 2005

## 3. Add Interaction factor( $k_{ij}$ ) as per Annex B

**Steel Design Code** ✕

Design Code : Eurocode3:05 ▼

National Annex : Recommended ▼

All Beams/Girders are Laterally Braced

Check Beam/Column Deflection

Apply Special Provisions for Seismic Design

Biaxial moments for buckling resistance

Biaxial moments at the same location

Maximum moments along the member

Consider as linear summation for class 1,2 (Eq. 6.2)

Method for interaction factor,  $k_{ij}$

By Code  Annex A  Annex B

Point of load application for  $M_{cr}$

Top  Shear Center  Bottom

The option on how to apply interaction factor ( $k_{ij}$ ) was added. In the previous version, only Annex A (Table A.1) was considered, but it has been improved to consider Annex B (Table B.1).

- "By Code" : It is automatically applied according to the recommended method for each National Annex.
  - In case of "Recommended", "Sweden", "Sweden(2019)", "Singapore", Annex A is applied.

### Annex A (Basic Equation)

**Table A.1: Interaction factors  $k_{ij}$  (6.3.3(4))**

| Interaction factors | Design assumptions   |  |
|---------------------|--|--|
|                     | elastic cross-sectional properties class 3, class 4        | plastic cross-sectional properties class 1, class 2  |
| $k_{yy}$            | $C_{my} C_{mLT} \frac{\mu_y}{1 - \frac{N_{Ed}}{N_{cr,y}}}$ | $C_{my} C_{mLT} \frac{\mu_y}{1 - \frac{N_{Ed}}{N_{cr,y}}} \frac{1}{C_{yy}}$                            |
| $k_{yz}$            | $C_{mz} \frac{\mu_y}{1 - \frac{N_{Ed}}{N_{cr,z}}}$         | $C_{mz} \frac{\mu_y}{1 - \frac{N_{Ed}}{N_{cr,z}}} \frac{1}{C_{yz}} 0,6 \sqrt{\frac{w_z}{w_y}}$         |
| $k_{zy}$            | $C_{my} C_{mLT} \frac{\mu_z}{1 - \frac{N_{Ed}}{N_{cr,y}}}$ | $C_{my} C_{mLT} \frac{\mu_z}{1 - \frac{N_{Ed}}{N_{cr,y}}} \frac{1}{C_{zy}} 0,6 \sqrt{\frac{w_y}{w_z}}$ |
| $k_{zz}$            | $C_{mz} \frac{\mu_z}{1 - \frac{N_{Ed}}{N_{cr,z}}}$         | $C_{mz} \frac{\mu_z}{1 - \frac{N_{Ed}}{N_{cr,z}}} \frac{1}{C_{zz}}$                                    |

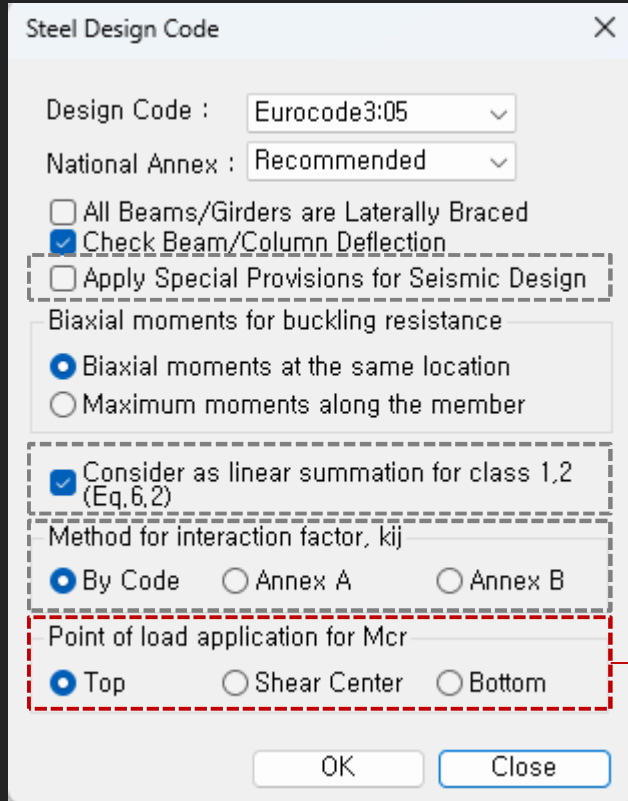
### Annex B (General Equation)

**Table B.1: Interaction factors  $k_{ij}$  for members not susceptible to torsional deformations**

| Interaction factors | Type of sections | Design assumptions   |   |
|---------------------|------------------|--|---|
|                     |                  | elastic cross-sectional properties class 3, class 4  | plastic cross-sectional properties class 1, class 2   |
| $k_{yy}$            | I-sections       | $C_{my} \left( 1 + 0,6 \bar{\lambda}_y \frac{N_{Ed}}{\chi_y N_{Rk} / \gamma_{M1}} \right)$ | $C_{my} \left( 1 + (\bar{\lambda}_y - 0,2) \frac{N_{Ed}}{\chi_y N_{Rk} / \gamma_{M1}} \right)$      |
|                     | RHS-sections     | $\leq C_{my} \left( 1 + 0,6 \frac{N_{Ed}}{\chi_y N_{Rk} / \gamma_{M1}} \right)$            | $\leq C_{my} \left( 1 + 0,8 \frac{N_{Ed}}{\chi_y N_{Rk} / \gamma_{M1}} \right)$                     |
| $k_{yz}$            | I-sections       | $k_{zz}$   | $0,6 k_{zz}$  |
| $k_{zy}$            | RHS-sections     | $0,8 k_{yy}$   | $0,6 k_{yy}$  |
| $k_{zz}$            | I-sections       | $C_{mz} \left( 1 + 0,6 \bar{\lambda}_z \frac{N_{Ed}}{\chi_z N_{Rk} / \gamma_{M1}} \right)$ | $C_{mz} \left( 1 + (2\bar{\lambda}_z - 0,6) \frac{N_{Ed}}{\chi_z N_{Rk} / \gamma_{M1}} \right)$     |
|                     | RHS-sections     | $\leq C_{mz} \left( 1 + 0,6 \frac{N_{Ed}}{\chi_z N_{Rk} / \gamma_{M1}} \right)$            | $\leq C_{mz} \left( 1 + 1,4 \frac{N_{Ed}}{\chi_z N_{Rk} / \gamma_{M1}} \right)$                     |
|                     |                  |  | $\leq C_{mz} \left( 1 + (\bar{\lambda}_z - 0,2) \frac{N_{Ed}}{\chi_z N_{Rk} / \gamma_{M1}} \right)$ |
|                     |                  |  | $\leq C_{mz} \left( 1 + 0,8 \frac{N_{Ed}}{\chi_z N_{Rk} / \gamma_{M1}} \right)$                     |

# Improved Steel Design as per EC3 : 2005

## 4. Calculation of M<sub>cr</sub> considering one-way symmetrical section and load position (only I-shape section)



- When calculating M<sub>cr</sub>, applying a general equation that can consider an axially symmetrical section and loading position has been improved.

### Basic Equation

(3) When  $k = k_w = 1,0$  (no end fixity):

$$M_{cr} = C_1 \frac{\pi^2 E I_z}{L^2} \left[ \frac{I_w}{I_z} + \frac{L^2 G I_t}{\pi^2 E I_z} \right]^{0.5}$$

### General Equation (New)

$$M_{cr} = C_1 \frac{\pi^2 E I_z}{(kL)^2} \left\{ \left[ \left( \frac{k}{k_w} \right)^2 \frac{I_w}{I_z} + \frac{(kL)^2 G I_t}{\pi^2 E I_z} + [C_2 z_g - C_3 z_j]^2 \right]^{0.5} - [C_2 z_g - C_3 z_j] \right\}$$

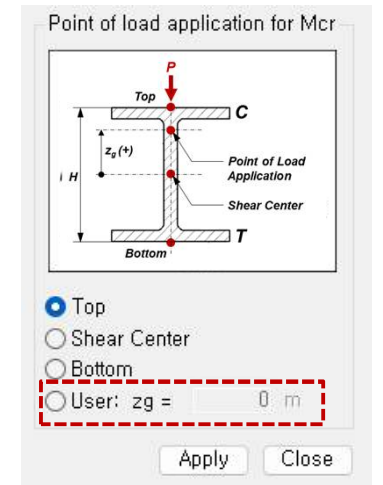
$$z_g = z_a - z_s$$

$$z_j = z_s - 0,5 \int_A (y^2 + z^2) z \, dA / I_y$$

$z_a$  is the coordinate of the point of load application

$z_s$  is the coordinate of the shear centre

- In the Steel Design dialog box, a batch setting of the loading point is supported. (for only Beam)
- Individual settings of loading position is supported in "Design Parameter>Point of load application for M<sub>cr</sub>" function.
  - ✓ User can input "z<sub>g</sub>" value. However, when inputting the value outside the cross-section, the value up to the edge of the cross-section is applied during design.
  - ✓ The top direction has a (+) sign.



# Wind loads

## 1. Added Wind loads as per ASCE7-16 & ASCE7-22

### Key Reflections

- ASCE 7 – 16 : “K<sub>e</sub>”(Ground Elevation adjustment Factor) was added to “q<sub>z</sub>” equation.

ASCE7-10  $q_z = 0.613K_zK_{zt}K_dV^2$  (N/m<sup>2</sup>); V in m/s

ASCE7-16  $q_z = 0.613K_zK_{zt}K_dK_eV^2$  (N/m<sup>2</sup>); V in m/s (26.10-1.si)

- ASCE 7 – 22

1. q<sub>z</sub> and p equations : “K<sub>d</sub>” was added to wind pressure(p) equation.

ASCE7-16  $q_z = 0.613K_zK_{zt}K_dK_eV^2$  (N/m<sup>2</sup>); V in m/s (26.10-1.si)  
 $p = q_h [(G_{cp}) - (GC_{pi})]$

ASCE7-22  $q_z = 0.00256K_hK_{zt}K_eV^2$   
 $p = q_h K_d [(G_{cp}) - (GC_{pi})]$

2. Modified Table 26.10-1 “K<sub>h</sub> and K<sub>z</sub> (Velocity pressure exposure Coefficients)” was reflected.

Add/Modify Wind Load Specification

Load Case Name : ventox

Wind Load Code : ASCE7(2016)

Description :

Wind Load Parameters

Basic Wind Speed : 85 mile/h

Exposure Category : C

Mean Roof Height : 27 m

Topographic Effects ...

Ground Elevation Factor: Kex 1 Key 1

Directional Factor : Kdx 0.85 Kdy 0.85

Rigid Structure  Flexible Structure

Gust Effect Factor : Gx 0.85 Gy 0.85 ...

Load Evaluation Using Force Coefficient

Force Coefficient : 1

Wind Eccentricity

X-Dir. (Wx) :  Positive  Negative  None

Y-Dir. (Wy) :  Positive  Negative  None

Wind Load Direction Factor (Scale Factor)

X-Dir, 1 Y-Dir, 0 Z-Rot, 0

Additional Wind Loads (Unit:kN,m)

| Story | Add.-X | Add.-Y | Add.-RZ |
|-------|--------|--------|---------|
|       |        |        |         |

Wind Load Profile... OK Cancel Apply

ASCE 7 - 16

Add/Modify Wind Load Specification

Load Case Name : ventox

Wind Load Code : ASCE7(2022)

Description :

Wind Load Parameters

Basic Wind Speed : 85 mile/h

Exposure Category : B

Mean Roof Height : 27 m

Topographic Effects ...

Ground Elevation Factor: Kex 1 Key 1

Directional Factor : Kdx 0.85 Kdy 0.85

Rigid Structure  Flexible Structure

Gust Effect Factor : Gx 0.85 Gy 0.85 ...

Load Evaluation Using Force Coefficient

Force Coefficient : 1

Wind Eccentricity

X-Dir. (Wx) :  Positive  Negative  None

Y-Dir. (Wy) :  Positive  Negative  None

Wind Load Direction Factor (Scale Factor)

X-Dir, 1 Y-Dir, 0 Z-Rot, 0

Additional Wind Loads (Unit:kN,m)

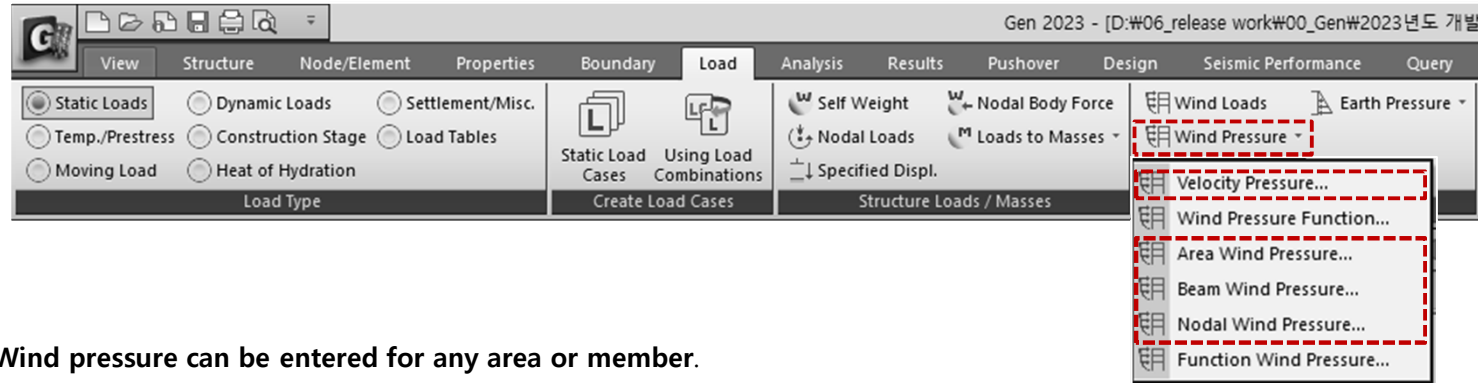
| Story | Add.-X | Add.-Y | Add.-RZ |
|-------|--------|--------|---------|
|       |        |        |         |

Wind Load Profile... OK Cancel Apply

ASCE 7 - 22

# Wind Pressure

## 1. Added Area/Beam/Nodal Wind Pressure in Wind Pressure feature



- Wind pressure can be entered for any area or member.

**Velocity Pressure:** Creates a Velocity Pressure function according to the code.

**Beam Wind Pressure:** Calculate the projected area of the selected beam element and input the wind load in the form of 'Element Beam Load.' The load applied at this time is applied as the projected area of the 1D element section, considering the loading angle.

**Area Wind Pressure:** Enter the wind load for a space frame structure with an arbitrary shape. If you select the 1D elements that make up the closed area, the wind load of the area is applied to each node as a nodal load.

**Nodal Wind Pressure:** Calculate the wind load acting on an arbitrary shape structure that is not included in the structural analysis model and apply it to the selected node.

# Wind Pressure

## 2. Beam Wind Pressure

- Calculate the projected area of the selected beam element and input the wind load in the form of 'Element Beam Load.' The load applied at this time is applied as the projected area of the 1D element section, considering the loading angle.

**Wind Pressure**

Beam Wind Pressure  ...

Load Case Name :  ...

Direction :

Angle :  [deg]

Scale Factor :

Wind Load Code :

Velocity Pressure Name :  ...

Ground Elevation Factor  $K_e$  :

Directional Factor  $K_d$  :

Gust Factor

External  $G_D$  :  ...

Internal  $G_{pi}$  :

Coefficient

Auto Calculate Coefficients ...

External  $C_f$  :

Internal  $C_f$  :

- Load Case Name** : Select the Load case.  
To enter, modify or delete additional load conditions, use the "...” button.
- Direction** : Select the direction of wind load action.  
\* X-Y : The load is applied in the horizontal direction of the structure (parallel to the X-Y plane of the global coordinate system).
- Angle** : Enter the wind load input angle about the global coordinate system X-axis.
- Scale factor** : Enter the increase/ decrease coefficient of wind load.
- Wind Load Code** : Select the standard for a calculation of wind pressure
  - ✓ ASCE7 (2022)
  - ✓ ASCE7 (2016)
  - ✓ KDS(41-12:2022)
  - ✓ KDS(41-10-15:2019)
  - ✓ KBC (2016)
  - ✓ KBC (2009)
  - ✓ China (GB50009-2012)
  - ✓ China (GB50009-2001)
- Velocity Pressure Name** : Select the function for a velocity pressure function.  
To add, modify or delete a velocity pressures, use the "...” button.
- Gust Factor** : Input a external and internal gust factor  
To calculate the gust factor automatically, use the "...”button.
- Coefficient**  
[Auto.Calculate Coefficients] : Check on it to calculate the coefficients automatically and Select the structure type.  
To calculate the external and internal  $C_f$  automatically, use the "...” button.
- Wind Pressure Profile...** : Show the wind pressure by the height from in a table and graph format.

## Wind Pressure

### 3. Area Wind Pressure

Enter the wind load for a space frame structure with an arbitrary shape. If you select the 1D elements that make up the closed area, the wind load of the area is applied to each node as a nodal load.

- Direction** : Select the direction of wind load action.
  - \* X-Y : The load is applied in the horizontal direction of the structure (parallel to the X-Y plane of the global coordinate system).
  - \* Normal: The load is applied perpendicular to the ground.
- Inner Pt.** : It is activated when Normal is selected in Direction field.
  - Selects the internal node of the structure.
  - When Inner Pt. is recognized as the inside of the structure and the load is inputted to the designated area, the load is applied from the outside to the inside of the structure.
- Wind Load Code** : Select the standard for a calculation of wind pressure (See "Beam Wind Pressure")
- Velocity Pressure Name** : Select the function for a velocity pressure function.
  - To add, modify or delete a velocity pressures, use the "... " button.
- Gust Factor** : Input a external and internal gust factor
  - To calculate the gust factor automatically, use the "... "button.
- Coefficient**
  - [Auto.Calculate Coefficients] : Check on it to calculate the coefficients automatically and Select the structure type.
  - To calculate the external and internal Cf automatically, use the "... " button.
- Selection** : Select the area where wind pressure will be applied. The selected area is calculated as the distributed wind load and the load will be applied on the nodes composing the area.
  - \* Group: Enter the load on the Area plane set in Loading Area Plane.
  - \* Element: Enter the load in the closed area created by the selected line element of the structure.
- Loading Area Group Name** : Select the Area Group which is defined from Structure> Group> Define Loading Area Group.
- Element Defining Loading Area** : Activated when the element is selected in the Selection field.
  - Select the line element composing the closed area.

# Wind Pressure

## 4. Nodal Wind Pressure

- Calculate the wind load acting on an arbitrary shape structure that is not included in the structural analysis model and apply it to the selected node.

**Wind Pressure**

Nodal Wind Pressure ...

Load Case Name : WL ...

Direction : X-Y ...

Angle : 0 [deg]

Scale Factor : 1

Wind Load Code : ASCE7(2022)

Velocity Pressure Name : Wind\_sign ...

Ground Elevation Factor  $K_e$  : 1.0000

Directional Factor  $K_d$  : 0.8500

Gust Factor

External GD : 2,2000 ...

Base Nodes for Structure : 2

Structure

Automatic ...

User Defined

Wind Direction Area : 12 m<sup>2</sup>

Concentrated Load point : 0, 0, 3 m

Wind Pressure Profile...

Apply Close

*Concentrated Load Point*

*Base Nodes*

[Example]

| Wall Pressure Coefficients, $C_p$ |            |       |          |
|-----------------------------------|------------|-------|----------|
| Surface                           | L/B        | $C_p$ | Use With |
| Windward wall                     | All values | 0.8   | $q_z$    |
|                                   | 0-1        | -0.5  | $q_h$    |
| Leeward wall                      | 2          | -0.3  | $q_h$    |
|                                   | $\geq 4$   | -0.2  | $q_h$    |
| Sidewall                          | All values | -0.7  | $q_h$    |

- Base Nodes for Structure** : Select or Input a nodes that support the wind load of the structure. The nodal load substituted with the wind load is input at the corresponding point.
- Structure** : Set the shape, area & action point for wind load calculation. Please refer to the figure above for the calculation.

**\* Automatic**

- It provides 4 basic shapes.
- Use after modifying the geometry's dimensions.
- The bottom center of the selected structure is set the average value of the X, Y coordinates and the highest Z level of the nodes selected in 'Base Nodes for Structure'.

**\* User Define**

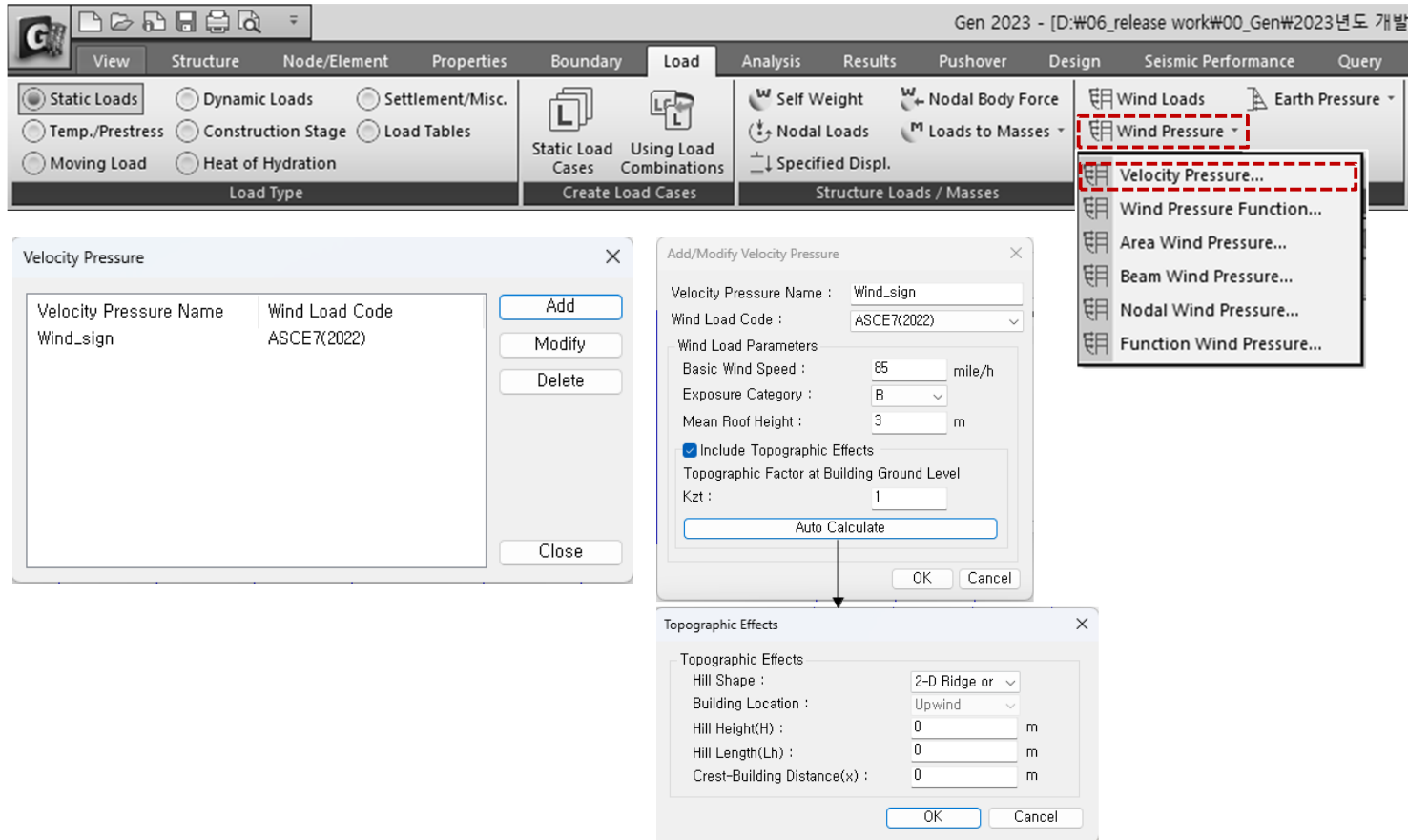
- Enter the loading area for the windward.
- Enter the centroid coordinate of the structure which the wind load is applied.

- $P = \text{Velocity Pressure} * \text{Area} * G * (C_{pw} - C_{pl})$
- $C_{pw} - C_{pl} = (0.8 - (-0.5)) = 1.3$
- $C_{pw}$  : Wall Pressure Coefficients of Windward
- $C_{pl}$  : Wall Pressure Coefficients of Leeward

# Wind Pressure

## 5. Velocity Pressure

Creates a Velocity Pressure function according to the code.



### Code to support the wind load

Select the standard for a calculation of wind pressure

- ASCE7 (2022)
- ASCE7 (2016)
- KDS(41-12:2022)
- KDS(41-10-15:2019)
- KBC (2016)
- KBC (2009)
- China (GB50009-2012)
- China (GB50009-2001)



# Wind Pressure

## 6. Improvement of Wind Pressure function

- Separation of Function and User's Input options

Add/Modify/Show Wind Pressure Function

Function  User's Input

Function Name : Eq Pi

Coordinate System : Cylindrical

Equation :  $(-9.12+(Z+Z)+0.013)+\cos(TH)$  ...  
 ( Example :  $0.7+Z+Z, \cos(TH)+R$  )

Description :

Table Show Option

Fixed Axis : R, TH Unit : m, [deg]

Z Start : 0 End : 9 Increment : 1

Fix Coordinates R 6 TH 180

Calculate

|    | R (m) | TH ((deg)) | Z (m) | Wind Pressure (kN/m <sup>2</sup> ) |
|----|-------|------------|-------|------------------------------------|
| 1  | 6     | 180        | 0     | 9.12                               |
| 2  | 6     | 180        | 1     | 9.107                              |
| 3  | 6     | 180        | 2     | 9.016                              |
| 4  | 6     | 180        | 3     | 8.769                              |
| 5  | 6     | 180        | 4     | 8.288                              |
| 6  | 6     | 180        | 5     | 7.495                              |
| 7  | 6     | 180        | 6     | 6.312                              |
| 8  | 6     | 180        | 7     | 4.661                              |
| 9  | 6     | 180        | 8     | 2.464                              |
| 10 | 6     | 180        | 9     | -0.357                             |

OK Cancel

Add/Modify/Show Wind Pressure Function

Function  User's Input

Function Name : Eq Pi

Coordinate System : Cylindrical

Equation :  $(-9.12+(Z+Z)+0.013)+\cos(TH)$  ...  
 ( Example :  $0.7+Z+Z, \cos(TH)+R$  )

Description :

Table Show Option

Fixed Axis : R, TH Unit : m, [deg]

Z Start : 0 End : 9 Increment : 1

Fix Coordinates R 6 TH 180

Calculate

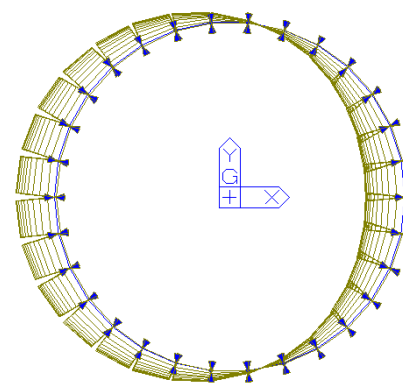
|    | R (m) | TH ((deg)) | Z (m) | Wind Pressure (kN/m <sup>2</sup> ) |
|----|-------|------------|-------|------------------------------------|
| 1  | 6     | 180        | 0     | 9.12                               |
| 2  | 6     | 180        | 1     | 9.107                              |
| 3  | 6     | 180        | 2     | 9.016                              |
| 4  | 6     | 180        | 3     | 8.769                              |
| 5  | 6     | 180        | 4     | 8.288                              |
| 6  | 6     | 180        | 5     | 7.495                              |
| 7  | 6     | 180        | 6     | 6.312                              |
| 8  | 6     | 180        | 7     | 4.661                              |
| 9  | 6     | 180        | 8     | 2.464                              |
| 10 | 6     | 180        | 9     | -0.357                             |

OK Cancel

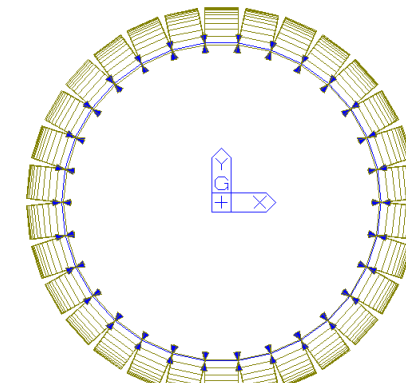
**[Note]**

When inputting wind pressure in the normal direction for a cylindrical shape, the input shape differs depending on the option of the function, as shown below. This is because "User's input" uses the entered value, so the input type shown on the left cannot be implemented.

[Function – Normal Direction]



[User's Input – Normal Direction]



**Function** → Automatically applied according to Equation

**User's Input** → You can modify "Wind Pressure" column in the table or paste an external value.

Finally, Input the loads to elements using the value entered in "Wind Pressure" column

\* User's Input is allowed Since the calculation function supported by Equation is limited.

# Rebar Detail Table

## 1. Support the Rebar detail table according to design provisions

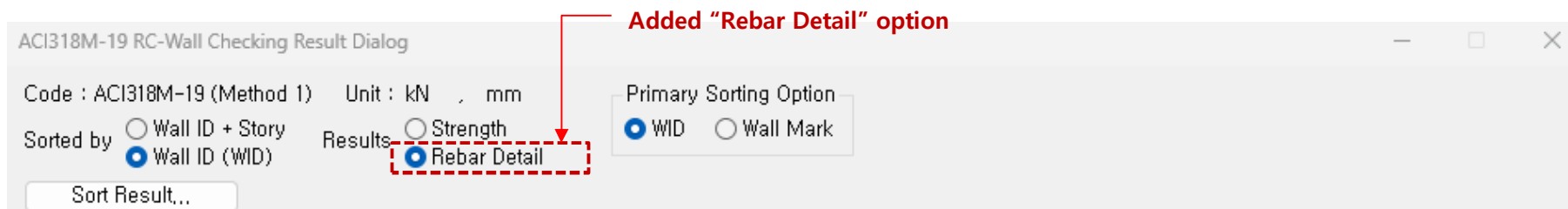
- It is supported only under "Code Checking" and outputs the checking result for the Min./Max. area of rebars or spacing between rebars required by the design code.

### Applied Code

- ACI 318(M) 14 & 19
- EC2 : 2004
- KDS 2022
- NSR-10
- NSCP 2015
- NTC-DCEC(2017)

### Column

- [Error Symbol in CHK column]  
 M : N.G. of Main rebar ratio  
 V : N.G. for Hoop  
 J : N.G. for Hoop in Joint



| MEMB | SEL                      | Section |       | fc      | fy      | CHK | Main Rebar (%) |       |       | Hoop |         |         |         |         |        |        |
|------|--------------------------|---------|-------|---------|---------|-----|----------------|-------|-------|------|---------|---------|---------|---------|--------|--------|
|      |                          | Bc      | Hc    | Height  | fys     |     | p.max          | p.use | p.min | POS  | Avy.use | Avy.min | Avz.use | Avz.min | s.max  | s.use  |
| 35   | <input type="checkbox"/> | rett0.4 |       | 0.03000 | 0.50000 | M   | 3.000          | 3.142 | 1.000 | End  | 398.10  | -       | 398.10  | -       | 320.00 | 100.00 |
| 1    | <input type="checkbox"/> | 400.0   | 400.0 | 3000.0  | 0.40000 |     |                |       |       | Mid  | 398.10  | -       | 398.10  | -       | 320.00 | 100.00 |

### Beam

- [Error Symbol in CHK column]  
 P : N.G. for rebar with Positive Moment  
 N : N.G. for rebar with Negative Moment  
 V : N.G. for Stirrup  
 T : N.G. for Sidebar with Torsion

| MEMB   | SEL                      | Section |       | fc      | POS | CHK | Main Rebar (Top) |           |           |        |        | Main Rebar (Bottom) |           |           |        |        | Stirrup |        |        |        |
|--------|--------------------------|---------|-------|---------|-----|-----|------------------|-----------|-----------|--------|--------|---------------------|-----------|-----------|--------|--------|---------|--------|--------|--------|
|        |                          | Bc      | Hc    | fy      |     |     | p.max (%)        | p.use (%) | p.min (%) | s.max  | s.use  | p.max (%)           | p.use (%) | p.min (%) | s.max  | s.use  | Av.use  | Av.min | s.max  | s.use  |
|        |                          | Span    | bf    | hf      |     |     | fys              |           |           |        |        |                     |           |           |        |        |         |        |        |        |
| 0      |                          | 600*600 |       | 0.03000 | I   | OK  | 1.895            | 0.390     | 0.280     | 185.45 | 157.67 | 1.895               | 0.390     | 0.223     | 185.45 | 157.67 | 1.3090  | 0.5250 | 268.25 | 120.00 |
| 4      | <input type="checkbox"/> | 600.0   | 600.0 | 0.50000 | M   | OK  | 1.895            | 0.390     | 0.074     | 185.45 | 157.67 | 1.895               | 0.390     | 0.200     | 185.45 | 157.67 | 0.8727  | 0.5250 | 268.25 | 180.00 |
| 5000.0 |                          | 0.000   | 0.000 | 0.40000 | J   | OK  | 1.895            | 0.390     | 0.280     | 185.45 | 157.67 | 1.895               | 0.390     | 0.111     | 185.45 | 157.67 | 1.3090  | 0.5250 | 268.25 | 120.00 |

### Wall

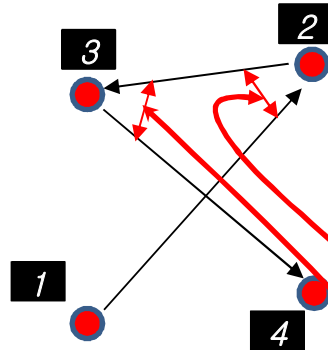
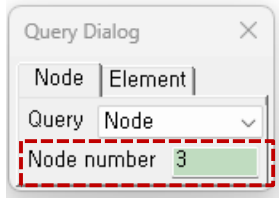
- [Error Symbol in CHK column]  
 V : N.G. for Vertical rebar  
 H : N.G. for Horizontal rebar  
 B : N.G. for Hoop in Boundary area

| WID | SEL                      | Wall Mark |        | fc      | fy      | CHK | V-Rebar  |          |          |        |        | H-Rebar  |          |        |        |  |  |  |  |
|-----|--------------------------|-----------|--------|---------|---------|-----|----------|----------|----------|--------|--------|----------|----------|--------|--------|--|--|--|--|
|     |                          | Lw        | HTw    | hw      | fys     |     | p.max(%) | p.use(%) | p.min(%) | s.max  | s.use  | p.use(%) | p.min(%) | s.max  | s.use  |  |  |  |  |
| 13  |                          | W3        |        | 0.03000 | 0.50000 |     |          |          |          |        |        |          |          |        |        |  |  |  |  |
| 1F  | <input type="checkbox"/> | 2500.0    | 3000.0 | 650.0   | 0.40000 | OK  | 4.000    | 0.595    | 0.250    | 450.00 | 100.00 | 0.345    | 0.250    | 450.00 | 70.000 |  |  |  |  |

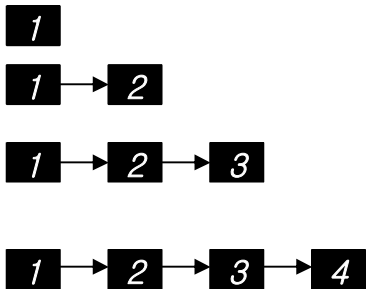
# Added Convenience functions

## 1. Angle information in Query Dialog

- In Query Dialog(Node), Provides angle information when clicking three or more nodes



### Order of clicks



```

Message Window
Node 5
Coordinates : X=10, Y=0, Z=0
Node 4
Coordinates : X=20, Y=0, Z=9
Distance from node 5 = 13.453624 (DX=10, DY=0, DZ=9)
Node 6
Coordinates : X=10, Y=0, Z=9
Distance from node 4 = 10 (DX=-10, DY=0, DZ=0), Angle = 41.987212°
Node 3
Coordinates : X=20, Y=0, Z=0
Distance from node 6 = 13.453624 (DX=10, DY=0, DZ=-9), Angle = 41.987212°
    
```

- Output only Coordinates of 1<sup>st</sup> node
- Output only Coordinates of 2<sup>nd</sup> node
- Output only Coordinates of 3<sup>rd</sup> node and Angle centered at previous node (2<sup>nd</sup> node)
- Output only Coordinates of 4<sup>th</sup> node and Angle centered at previous node (3<sup>rd</sup> node)

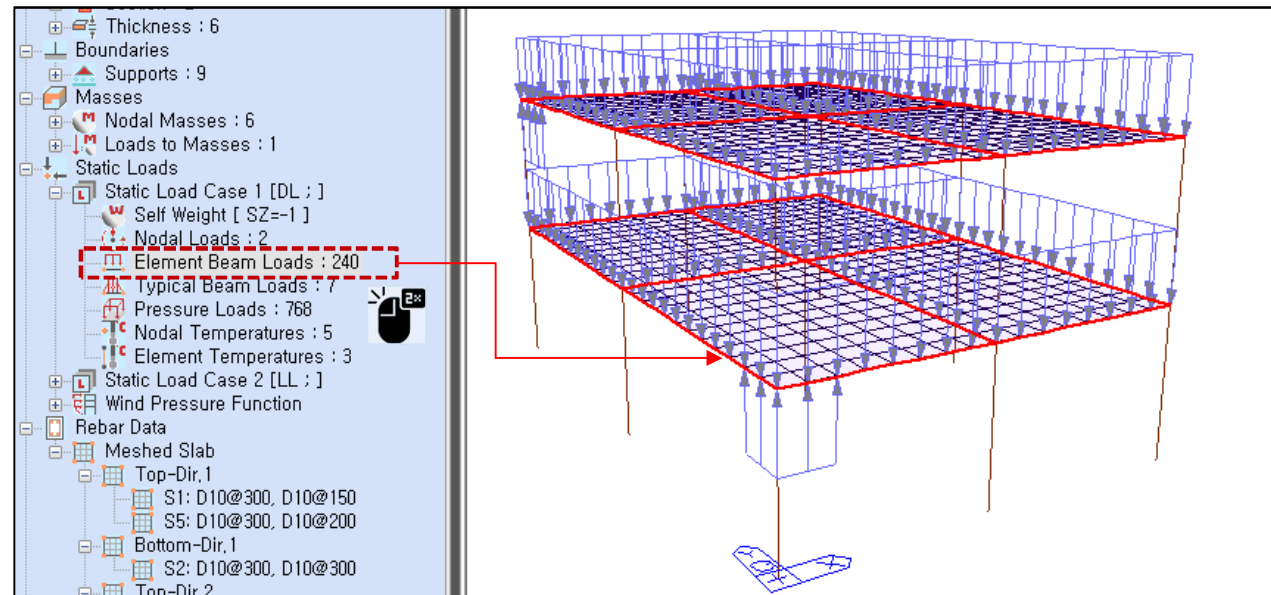
## Added Convenience functions

### 2. Objects selection by load information

- Select elements or nodes to which load is assigned → When double-clicking a loads in the work tree, the objects to which the load is assigned is selected.

**The target load is as follows.**

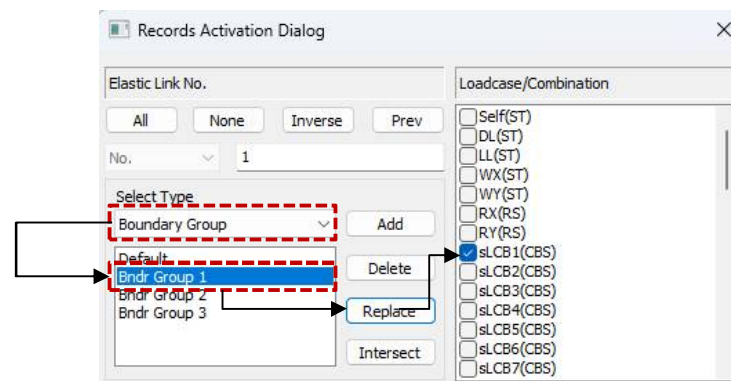
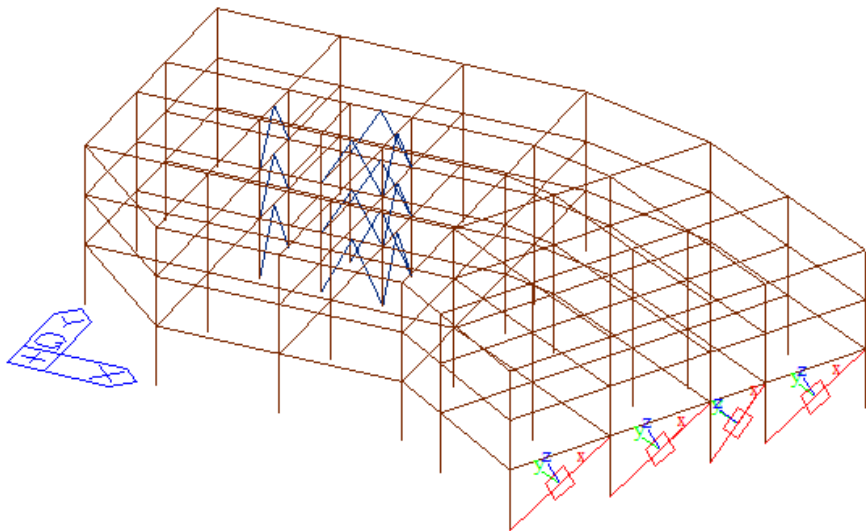
- *Nodal load*
- *Beam Load (Element beam load, Typical Beam load)*
- *Pressure load*
- *Specified Displacements of supports*
- *Temperatures (Element Temperatures, Nodal Temperatures)*



## Added Convenience functions

### 3. Improvement of Elastic & General Link Table

- Link result output support by Boundary Group



- Step 01 : Select "Boundary Group".
- Step 02 : Select Target Group Name.
- Step 03 : Click "Replace".
- Step 04 ; Select target load cases or load combinations
- Step 05 : Click "OK"

| No | Node1 | Node2 | Type | RIGID  | SDx (kN/m) | Distance Ratio SDy | Distance Ratio SDz | Group        |
|----|-------|-------|------|--------|------------|--------------------|--------------------|--------------|
| 1  | 60    | 26    | GE   | 000000 | 10000.0000 | 0.50               | 0.50               | Bndr Group 1 |
| 2  | 61    | 28    | GE   | 000000 | 10000.0000 | 0.50               | 0.50               | Bndr Group 2 |
| 3  | 63    | 30    | GE   | 000000 | 10000.0000 | 0.50               | 0.50               | Bndr Group 3 |
| 4  | 65    | 32    | GE   | 000000 | 10000.0000 | 0.50               | 0.50               | Bndr Group 3 |

[Elastic Link Table]

| No. | Load  | Node | Axial (kN) | Shear-y (kN) | Shear-z (kN) | Torsion (kN-m) | Moment-y (kN-m) | Moment-z (kN-m) |
|-----|-------|------|------------|--------------|--------------|----------------|-----------------|-----------------|
| 1   | sLCB1 | 60   | -5.38      | 0.00         | 0.00         | 0.00           | 0.00            | 0.00            |
| 1   | sLCB1 | 26   | -5.38      | 0.00         | 0.00         | 0.00           | 0.00            | 0.00            |

[Output results for the selected group]

# Irregularity Check according to NTC 2022 [NTC-DCEC (2017)]

## 1. Torsional Irregularity & Weight Irregularity

- Results > Results Tables > Story> Torsional, Weight, Stiffness, and Capacity Irregularity Check

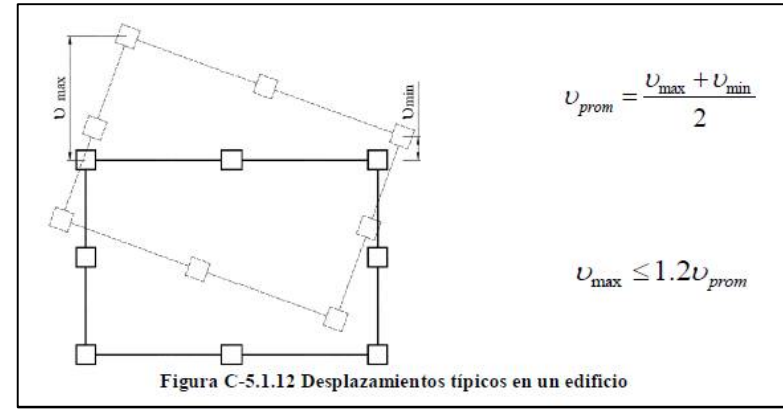
| Torsional Irregularity Check |       |           |                  |                                 |                     |               |                 |         |  |
|------------------------------|-------|-----------|------------------|---------------------------------|---------------------|---------------|-----------------|---------|--|
| Load Case                    | Story | Level (m) | Story Height (m) | Average Value of Extreme Points |                     | Maximum Value |                 | Remark  |  |
|                              |       |           |                  | Story Drift (m)                 | 1.2*Story Drift (m) | Node          | Story Drift (m) |         |  |
| Rx(RS)                       | 9F    | 32.50     | 4.00             | 0.0085                          | 0.0102              | 161           | 0.0085          | Regular |  |
| Rx(RS)                       | 8F    | 28.50     | 4.00             | 0.0123                          | 0.0148              | 156           | 0.0123          | Regular |  |
| Rx(RS)                       | 7F    | 24.50     | 4.00             | 0.0129                          | 0.0154              | 121           | 0.0129          | Regular |  |
| Rx(RS)                       | 6F    | 20.50     | 4.00             | 0.0134                          | 0.0160              | 116           | 0.0134          | Regular |  |
| Rx(RS)                       | 5F    | 16.50     | 4.00             | 0.0149                          | 0.0178              | 96            | 0.0149          | Regular |  |
| Rx(RS)                       | 4F    | 12.50     | 4.00             | 0.0133                          | 0.0159              | 61            | 0.0133          | Regular |  |
| Rx(RS)                       | 3F    | 8.50      | 4.00             | 0.0119                          | 0.0143              | 56            | 0.0119          | Regular |  |
| Rx(RS)                       | 2F    | 4.50      | 4.00             | 0.0119                          | 0.0143              | 21            | 0.0119          | Regular |  |
| Rx(RS)                       | 1F    | 0.00      | 4.50             | 0.0103                          | 0.0123              | 16            | 0.0103          | Regular |  |
| Ry(RS)                       | 9F    | 32.50     | 4.00             | 0.0063                          | 0.0076              | 180           | 0.0063          | Regular |  |
| Ry(RS)                       | 8F    | 28.50     | 4.00             | 0.0066                          | 0.0080              | 160           | 0.0066          | Regular |  |
| Ry(RS)                       | 7F    | 24.50     | 4.00             | 0.0066                          | 0.0080              | 140           | 0.0066          | Regular |  |
| Ry(RS)                       | 6F    | 20.50     | 4.00             | 0.0065                          | 0.0078              | 120           | 0.0065          | Regular |  |
| Ry(RS)                       | 5F    | 16.50     | 4.00             | 0.0062                          | 0.0075              | 100           | 0.0062          | Regular |  |
| Ry(RS)                       | 4F    | 12.50     | 4.00             | 0.0055                          | 0.0066              | 80            | 0.0055          | Regular |  |
| Ry(RS)                       | 3F    | 8.50      | 4.00             | 0.0044                          | 0.0053              | 60            | 0.0044          | Regular |  |
| Ry(RS)                       | 2F    | 4.50      | 4.00             | 0.0034                          | 0.0041              | 40            | 0.0034          | Regular |  |
| Ry(RS)                       | 1F    | 0.00      | 4.50             | 0.0021                          | 0.0025              | 20            | 0.0021          | Regular |  |

| Weight Irregularity Check |       |           |                  |                   |                  |                    |         |  |
|---------------------------|-------|-----------|------------------|-------------------|------------------|--------------------|---------|--|
| Load Case                 | Story | Level (m) | Story Height (m) | Story Weight (kN) | Adjacent Story   | Story Weight Ratio | Remark  |  |
|                           |       |           |                  |                   | 1.2M(Lower) (kN) |                    |         |  |
| Rx(RS)                    | Roof  | 36.50     | 0.00             | 4641.229          | 7874.492         | 0.000              | -       |  |
| Rx(RS)                    | 9F    | 32.50     | 4.00             | 6562.077          | 7988.095         | 0.821              | Regular |  |
| Rx(RS)                    | 8F    | 28.50     | 4.00             | 6656.746          | 8740.032         | 0.762              | Regular |  |
| Rx(RS)                    | 7F    | 24.50     | 4.00             | 7283.360          | 8740.032         | 0.833              | Regular |  |
| Rx(RS)                    | 6F    | 20.50     | 4.00             | 7283.360          | 8832.198         | 0.825              | Regular |  |
| Rx(RS)                    | 5F    | 16.50     | 4.00             | 7360.165          | 9731.187         | 0.756              | Regular |  |
| Rx(RS)                    | 4F    | 12.50     | 4.00             | 8109.323          | 9803.678         | 0.827              | Regular |  |
| Rx(RS)                    | 3F    | 8.50      | 4.00             | 8169.732          | 9908.531         | 0.825              | Regular |  |
| Rx(RS)                    | 2F    | 4.50      | 4.00             | 8257.109          | 0.000            | 0.000              | Regular |  |
| Rx(RS)                    | 1F    | 0.00      | 4.50             | 786.395           | 0.000            | 0.000              | -       |  |

✓ Note

### 1. Torsional Irregularity Check

According to Section 5.1. 12) in NTCS2020, "Story Drift of Maximum Value" divided by "1.2\*Story Drift of Average Value of Extreme Points." If it exceeds 1.0, "Irregular" is printed. If it is less than 1.0, 'Regular' is printed.



### 2. Weight Irregularity Check

According to Section 5.1. 7) in NTCS2020, "Story Weight Ratio", Story Weight divided by 1.2\*Story Weight of adjacent lower story, If it exceeds 1.0, "Irregular" is printed. If it is less than 1.0, 'Regular' is printed.

# Irregularity Check according to NTC 2022 [NTC-DCEC (2017)]

## 2. Stiffness Irregularity

- Results > Results Tables > Story> Torsional, Weight , Stiffness, and Capacity Irregularity Check

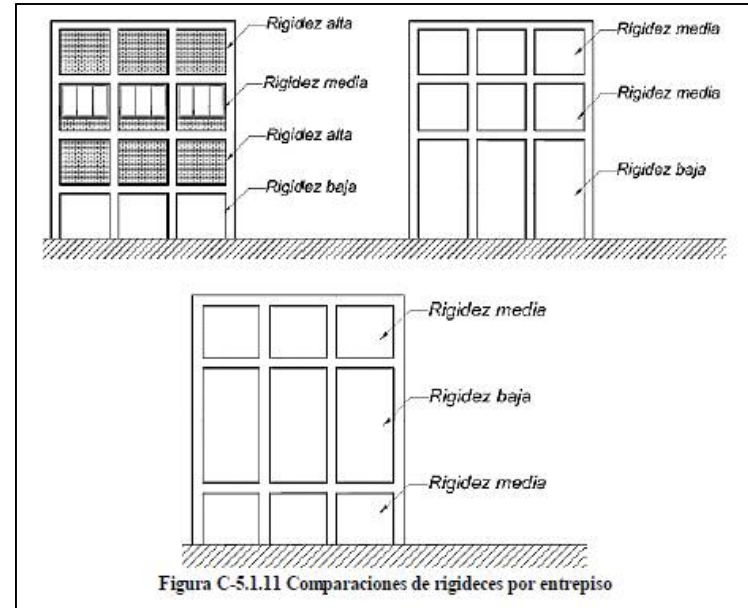
### Stiffness Irregularity Check

|   | Load Case | Story | Level (m) | Story Height (m) | Story Drift (m) | Story Shear Force (kN) | Story Stiffness | Lower Story Stiffness |              | Remark    |
|---|-----------|-------|-----------|------------------|-----------------|------------------------|-----------------|-----------------------|--------------|-----------|
|   |           |       |           |                  |                 |                        |                 | 1.2K (Lower)          | 0.8K (Lower) |           |
| ▶ | Rx(RS)    | 9F    | 32.50     | 4.00             | 0.0085          | 1739.04                | 471.65          | 389.03                | 259.35       | Irregular |
|   | Rx(RS)    | 8F    | 28.50     | 4.00             | 0.0123          | 3825.51                | 324.19          | 373.23                | 248.82       | Regular   |
|   | Rx(RS)    | 7F    | 24.50     | 4.00             | 0.0129          | 5597.45                | 311.03          | 358.98                | 239.32       | Regular   |
|   | Rx(RS)    | 6F    | 20.50     | 4.00             | 0.0134          | 7239.69                | 299.15          | 323.01                | 215.34       | Regular   |
|   | Rx(RS)    | 5F    | 16.50     | 4.00             | 0.0149          | 8611.13                | 269.17          | 361.70                | 241.14       | Regular   |
|   | Rx(RS)    | 4F    | 12.50     | 4.00             | 0.0133          | 9695.44                | 301.42          | 401.94                | 267.96       | Regular   |
|   | Rx(RS)    | 3F    | 8.50      | 4.00             | 0.0119          | 10601.04               | 334.95          | 401.83                | 267.89       | Regular   |
|   | Rx(RS)    | 2F    | 4.50      | 4.00             | 0.0119          | 11235.88               | 334.86          | 526.35                | 350.90       | Irregular |
|   | Rx(RS)    | 1F    | 0.00      | 4.50             | 0.0103          | 11556.30               | 438.63          | 0.00                  | 0.00         | -         |

✓ Note

### 3. Stiffness Irregularity(Soft Story) Check

According to Section 5.1. 11) in NTCS2020,  
 When the story stiffness of a particular story is greater than 1.2 times or lower than 0.8 times the stiffness of the story below, then the story will be defined as irregular.



# Irregularity Check according to NTC 2022 [NTC-DCEC (2017)]

## 3. Capacity Irregularity

**Capacity Irregularity Check**

| Load Case | Story | Level (m) | X-Direction            |                           |                        |           | Y-Direction            |                           |                        |           |
|-----------|-------|-----------|------------------------|---------------------------|------------------------|-----------|------------------------|---------------------------|------------------------|-----------|
|           |       |           | Story Shear Force (kN) | Story Shear Strength (kN) | Strength / Force Ratio | Remark    | Story Shear Force (kN) | Story Shear Strength (kN) | Strength / Force Ratio | Remark    |
| Rx(RS)    | 9F    | 32.50     | 1739.04                | 10045.0635                | 5.7762                 | -         | 0.00                   | 16874.3031                | -                      | -         |
| Rx(RS)    | 8F    | 28.50     | 3825.51                | 10045.0635                | 2.6258                 | Regular   | 0.00                   | 16874.3031                | -                      | -         |
| Rx(RS)    | 7F    | 24.50     | 5597.45                | 20534.6914                | 3.6686                 | Regular   | 0.00                   | 26293.4714                | -                      | -         |
| Rx(RS)    | 6F    | 20.50     | 7239.69                | 20534.6914                | 2.8364                 | Regular   | 0.00                   | 26293.4714                | -                      | -         |
| Rx(RS)    | 5F    | 16.50     | 8611.13                | 20534.6914                | 2.3847                 | Irregular | 0.00                   | 26293.4714                | -                      | -         |
| Rx(RS)    | 4F    | 12.50     | 9695.44                | 30145.8695                | 3.1093                 | Regular   | 0.00                   | 36296.9646                | -                      | -         |
| Rx(RS)    | 3F    | 8.50      | 10601.04               | 30145.8695                | 2.8437                 | Regular   | 0.00                   | 36881.8779                | -                      | -         |
| Rx(RS)    | 2F    | 4.50      | 11235.88               | 30145.8695                | 2.6830                 | Regular   | 0.00                   | 36881.8779                | -                      | -         |
| Rx(RS)    | 1F    | 0.00      | 11556.30               | 30145.8695                | 2.6086                 | Regular   | 0.00                   | 36881.8779                | -                      | -         |
| Ry(RS)    | 9F    | 32.50     | 0.00                   | 10045.0635                | -                      | -         | 1791.60                | 16874.3031                | 9.4185                 | -         |
| Ry(RS)    | 8F    | 28.50     | 0.00                   | 10045.0635                | -                      | -         | 3814.81                | 16874.3031                | 4.4234                 | Regular   |
| Ry(RS)    | 7F    | 24.50     | 0.00                   | 20534.6914                | -                      | -         | 5451.67                | 26293.4714                | 4.8230                 | Regular   |
| Ry(RS)    | 6F    | 20.50     | 0.00                   | 20534.6914                | -                      | -         | 6886.75                | 26293.4714                | 3.8180                 | Regular   |
| Ry(RS)    | 5F    | 16.50     | 0.00                   | 20534.6914                | -                      | -         | 8022.24                | 26293.4714                | 3.2776                 | Irregular |
| Ry(RS)    | 4F    | 12.50     | 0.00                   | 30145.8695                | -                      | -         | 8889.64                | 36296.9646                | 4.0831                 | Regular   |
| Ry(RS)    | 3F    | 8.50      | 0.00                   | 30145.8695                | -                      | -         | 9568.04                | 36881.8779                | 3.8547                 | Regular   |
| Ry(RS)    | 2F    | 4.50      | 0.00                   | 30145.8695                | -                      | -         | 10006.88               | 36881.8779                | 3.6857                 | Regular   |
| Ry(RS)    | 1F    | 0.00      | 0.00                   | 30145.8695                | -                      | -         | 10215.02               | 36881.8779                | 3.6106                 | Regular   |

Select Calculation Method

Country Code : NTC2020

Story Drift Method

- Drift at the Center of Mass
- Max. Drift of Outer Extreme Points
- Max. Drift of All Vertical Elements

Story Stiffness Method

- 1 / Story Drift Ratio
- Story Shear / Story Drift

Seismic Behavior Factor, Q

- Q = 4
- Q ≤ 3

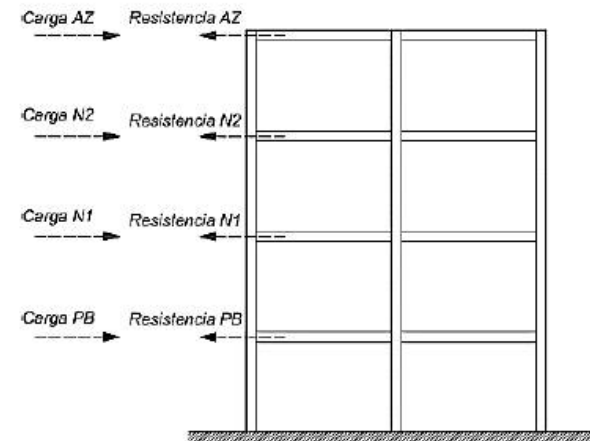
OK Cancel

✓ You can set the seismic behavior factor, Q in Irregularity Check Parameter Dialog Box.

✓ Note

### 4. Capacity Irregularity (Weak Story) check

According to Section 5.1. 13) in NTCS2020, In systems designed for  $Q=4$  or  $Q \leq 3$ , the ratio of lateral load resisting capacity to the design action in any story must not be less than 85 percent or 75 percent of the average of these ratios for all stories, respectively. If it exceeds 1.0, "Irregular" is printed. If it is less than 1.0, 'Regular' is printed. This requirement excludes the last story.



Si  $Q = 4$  entonces no se debe cumplir que

$$\frac{\text{Resistencia entrepiso } i}{\text{Carga entrepiso } i} < 0.85 \text{ Promedio } \frac{\text{Resistencia entrepisos}}{\text{Carga entrepisos}}$$

Si  $Q \leq 3$  entonces no se debe cumplir que

$$\frac{\text{Resistencia entrepiso } i}{\text{Carga entrepiso } i} < 0.75 \text{ Promedio } \frac{\text{Resistencia entrepisos}}{\text{Carga entrepisos}}$$

Figura C-5.1.13 Condiciones de resistencias y cargas laterales



# Gen-Revit 2024 Linker

- File > Import > midas Gen MGT File
- File > Export > midas Gen MGT File (It is mgt file to update the Revit model)

The image shows two software windows. The top window is 'User-defined Section Mapping' with a table:

| Mapping Method | Revit Family Name | Revit Type Name             | Civil Code | Civil Shape | Civil Section Name |        |
|----------------|-------------------|-----------------------------|------------|-------------|--------------------|--------|
| 1              | NAME              | Flangia larga ad H-Pilastro | HE100A     | UNI         | H                  | HEA100 |
| 2              | NAME              | Flangia larga ad H-Pilastro | HE120A     | UNI         | H                  | HEA120 |
| 3              | NAME              | Flangia larga ad H-Pilastro | HE140A     | UNI         | H                  | HEA140 |
| 4              | NAME              | Flangia larga ad H-Pilastro | HE160A     | UNI         | H                  | HEA160 |
| 5              | NAME              | Flangia larga ad H-Pilastro | HE180A     | UNI         | H                  | HEA180 |
| 6              | NAME              | Flangia larga ad H-Pilastro | HE200A     | UNI         | H                  | HEA200 |
| 7              | NAME              | Flangia larga ad H-Pilastro | HE220A     | UNI         | H                  | HEA220 |

The bottom window is 'Send Model to midas Civil' with fields for Revit Model, Civil Model, Element Size, Export Target, Unit, Force, Length, Section Mapping, and Material Mapping.

**Send Model to midas Gen**

|                         | Functions                   | Revit ↔ Gen |
|-------------------------|-----------------------------|-------------|
| <b>Linear Elements</b>  | Structural Column           | ↔           |
|                         | Beam                        | ↔           |
|                         | Brace                       | ↔           |
|                         | Curved Beam                 | >           |
|                         | Beam System                 | >           |
|                         | Truss                       | >           |
| <b>Planar Elements</b>  | Foundation Slab             | ↔           |
|                         | Structural Floor            | ↔           |
|                         | Structural Wall             | ↔           |
|                         | Wall Opening & Window       | >           |
|                         | Door                        | >           |
|                         | Vertical or Shaft Opening   | >           |
|                         | Offset                      | >           |
|                         | Rigid Link                  | >           |
|                         | Cross-Section Rotation      | >           |
|                         | End Release                 | >           |
| <b>Boundary</b>         | Isolated Foundation Support | >           |
|                         | Point Boundary Condition    | >           |
|                         | Line Boundary Condition     | >           |
|                         | Wall Foundation             | >           |
|                         | Area Boundary Condition     | >           |
|                         | Load Nature                 | >           |
|                         | Load Case                   | >           |
| <b>Load</b>             | Load Combination            | >           |
|                         | Hosted Point Load           | >           |
|                         | Hosted Line Load            | >           |
|                         | Hosted Area Load            | >           |
|                         | Material                    | ↔           |
| <b>Other Parameters</b> | Level                       | >           |

The image shows two software windows side-by-side. The left window is 'Revit 2024' showing a 3D model of a building. The right window is 'Gen2024 v1.1 (New version)' showing a 3D model of the same building with a blue circular arrow icon between them, indicating a link or transfer process.

✓ Note

In Revit 2023, only elements created as structural elements through “Analytical Automation” function can be exported to Gen.

At this time, load and geometric information are ignored.

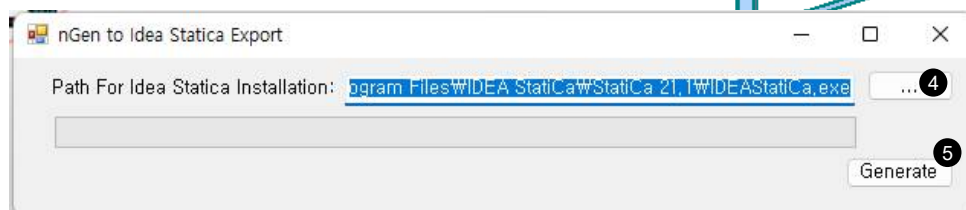
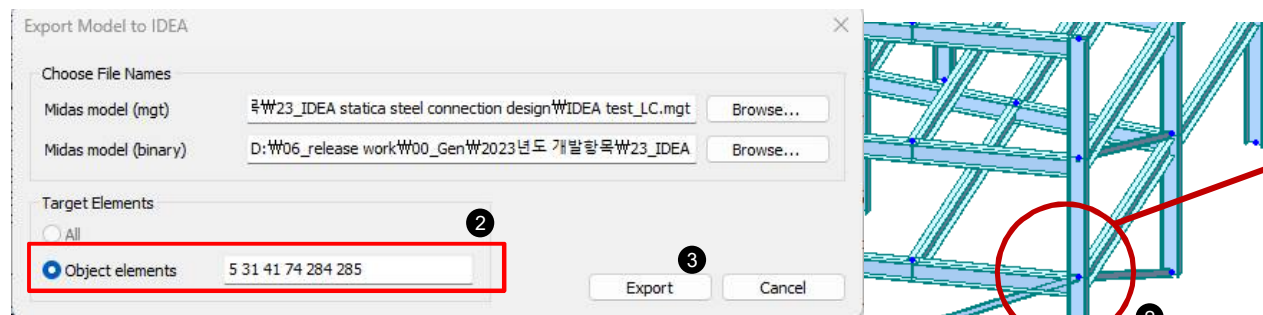
The screenshot shows the 'Analytical Automation' dialog box with the following settings:

- 1. Select physical elements: Total Elements: 4 (checked)
- 2.1. Adjust analytical elements using connectivity rules: False
- 2.2. Tolerance of the distance between analytical elements: 0.35
- 3.1. Adjust analytical elements to nearest level: False
- 3.2. Tolerance of the distance to the nearest level: 0.5
- 4.1. First group of elements considered for adjustment: Wall
- 4.2. Second group of elements considered for adjustment: Column

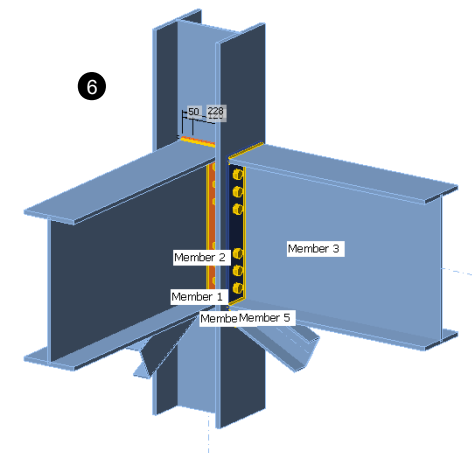
## Interface for Gen - IDEA Statica Connection

1. Through the link of Gen - IDEA Statica Connection, Various joint design can be performed.

- File > Export > IDEA Steel Connection



**\* It is supported since IDEA Statica 23.0**



- 1 Run "Steel Connection Export."
- 2 Select members connected with a specific target point (connection)
- 3 Click "Export" and Save it as a and "\*.mgt" and "\*.mid" file.
- 4 Click "..." and Link "IDEAStatica.exe" file.
- 5 Click "Generate" and Check the model in IDEA Statica Connection.
- 6 Perform Joint modeling and design in IDEA Statica Connection.

### Note )

Since the design member force needs to be exported, it can be used after analysis and design are completed in Gen.

User's defined sections are not supported. (Only the sections in DB are exported normally.)

# Interface for Gen - IDEA Statica Connection

1. Through the link of Gen - IDEA Statica Connection, Various joint design can be performed.

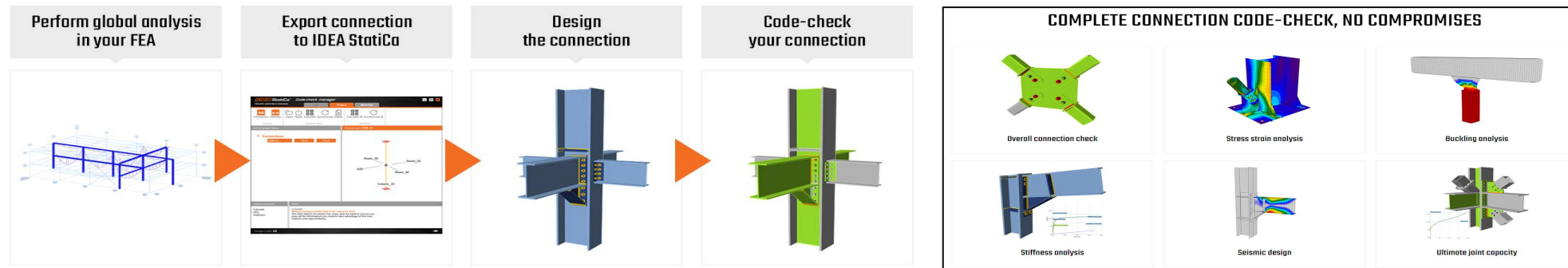
- File > Export > IDEA Steel Connection

• **Exported Data**

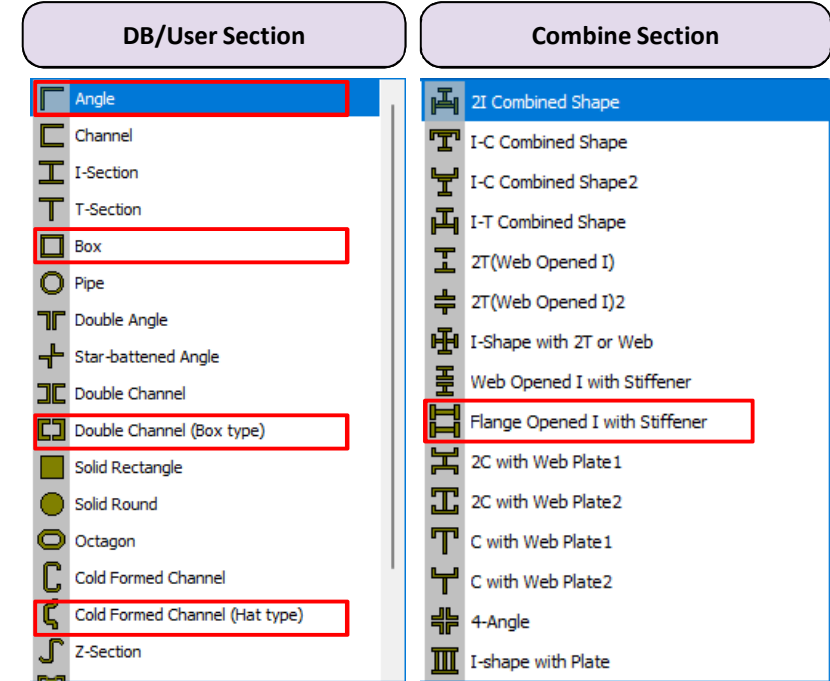
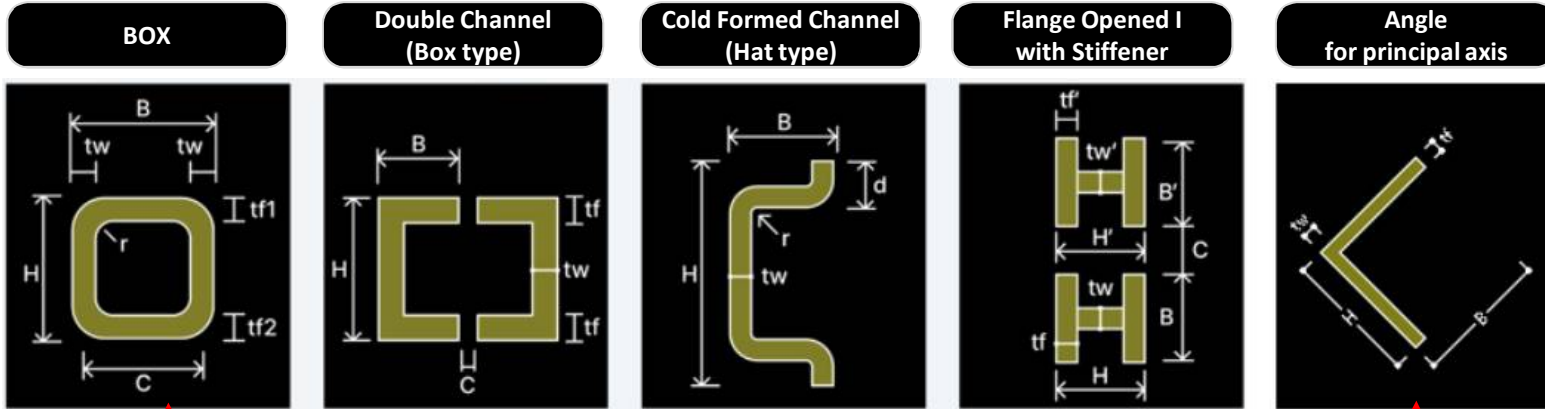
*\* It is supported since IDEA Statica 23.0*

| Item           | Exported                            | Detail   |
|----------------|-------------------------------------|--|
| Unit           | <input type="radio"/>               | Convert units automatically  |
| Section        | <input type="radio"/>               | I-Shape, Angel, Double Angel, T-Shape, Double T-Shape, Double Channel, Box, Pipe<br>* Note : Unsupported sections are replaced with I-Shape. |
| Material       | <input type="radio"/>               | -  |
| Section Offset | <input checked="" type="checkbox"/> | User should set the offset data in IDEA Statica Connection   |
| Member Force   | <input type="radio"/>               | Design forces of both ends are exported as member force of IDEA.   |
| Design Code    | <input type="radio"/>               | EC3:2005, AISC   |

• **IDEA Statica** : <https://www.ideastatica.com/connection-design>



# Add New Sections



DB/User | Value | SRC | Combined | Tapered | Composite

Section ID: 4

Name: 1

Sect. Name: [ ]

Get Data from Single Angle

DB Name: AISC10(US)

Sect. Name: [ ]

|     |   |   |
|-----|---|---|
| H   | 0 | m |
| B   | 0 | m |
| tw  | 0 | m |
| tf1 | 0 | m |
| C   | 0 | m |
| tf2 | 0 | m |
| B1  | 0 | m |
| B2  | 0 | m |
| r   | 0 | m |

Round type

Add "round" option in Box

DB/User | Value | SRC | Combined | Tapered | Composite

Section ID: 4

Name: 1

Sect. Name: [ ]

Get Data from Single Angle

DB Name: AISC10(US)

Sect. Name: [ ]

|    |       |   |
|----|-------|---|
| H  | 0.025 | m |
| B  | 0.025 | m |
| tw | 0.004 | m |
| tf | 0.004 | m |

Consider Principal Axis

theta: 45 [deg]

Add "Consider Principal Axis" option in Angle

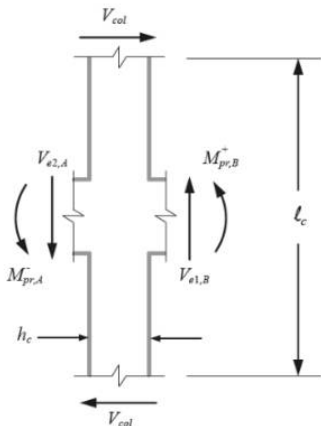
**Note**

- Design is not supported for the additional sections.
- In case of Angle for principal axis, the section properties are calculated by FEM method.

ETC.

| Items   | Detail  | Design Code                                   |                   |                 |                        |             |   |                                      |   |                         |       |        |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
|---|---|---|-------------------|-----------------|------------------------|-------------|---|--------------------------------------|---|-------------------------|-------|--------|--|-----|-----|--|--|--|-----|--|--|--|-------------|---------------|------|--------|-------------|---------------|------|--------|--|--|--|--|--|--|--|--|--|--|--|--|--|---|--|--|--|--|--|--|--|--|--|--|--|--|--|-----|-------|---------|-----------------|--------|----------|-------|----|--------|-----------|-------|----|--|-----|-------|---------|-----------------|--------|----------|-------|----|--------|-----------|-------|----|--|-----|-------|---------|-----------------|---------|----------|-------|----|--------|-----------|-------|----|--|-----|-------|---------|-----------------|---------|----------|-------|----|--------|-----------|-------|----|--|
| <p>Max. spacing (<math>s_{max}</math>)<br/>of tensile rebars in Beam design</p>   | <ul style="list-style-type: none"> <li>Apply 'fs' calculated by service load combinations</li> <li>* Only "2/3*fy" is considered only in a beam design of Gen.</li> </ul> <table border="1" data-bbox="901 382 1556 619"> <thead> <tr> <th>Reinforcement type</th> <th colspan="2">Maximum spacing s</th> </tr> </thead> <tbody> <tr> <td rowspan="2">Deformed bars or wires</td> <td rowspan="2">Lesser of:</td> <td><math>380 \left( \frac{280}{f_s} \right) - 2.5e_c</math></td> </tr> <tr> <td><math>300 \left( \frac{280}{f_s} \right)</math></td> </tr> </tbody> </table> <div data-bbox="901 644 1574 782"> <p><input checked="" type="checkbox"/> Check the interaction for biaxial shear</p> <p>fs of Main bar in Beam Design</p> <p><input type="radio"/> 2/3*fy      <input checked="" type="radio"/> By Program</p> </div>  | Reinforcement type                            | Maximum spacing s |                 | Deformed bars or wires | Lesser of:  | $380 \left( \frac{280}{f_s} \right) - 2.5e_c$ | $300 \left( \frac{280}{f_s} \right)$ | <ul style="list-style-type: none"> <li>ACI 318(M) 14 &amp; 19</li> <li>KDS 2022</li> <li>NSR-10</li> <li>NSCP 2015</li> <li>NTC-DCEC(2017)</li> </ul> |                         |       |        |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
| Reinforcement type  | Maximum spacing s   |   |                   |                 |                        |             |   |                                      |   |                         |       |        |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
| Deformed bars or wires  | Lesser of:  | $380 \left( \frac{280}{f_s} \right) - 2.5e_c$ |                   |                 |                        |             |   |                                      |   |                         |       |        |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
|   |   | $300 \left( \frac{280}{f_s} \right)$          |                   |                 |                        |             |   |                                      |   |                         |       |        |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
| <p>Cyclic Shear Resistance table</p>  | <ul style="list-style-type: none"> <li>"Load" column is added. (Output the most unfavorable load combination.)</li> </ul> <table border="1" data-bbox="723 893 1857 1179"> <thead> <tr> <th rowspan="3"></th> <th rowspan="3">Elem</th> <th rowspan="3">Location</th> <th rowspan="3">Seismic Element</th> <th rowspan="3">Load</th> <th colspan="8">Cyclic Shear Resistance</th> </tr> <tr> <th colspan="4">VRy</th> <th colspan="4">VRz</th> </tr> <tr> <th>Demand (kN)</th> <th>Capacity (kN)</th> <th>Load</th> <th>Remark</th> <th>Demand (kN)</th> <th>Capacity (kN)</th> <th>Load</th> <th>Remark</th> </tr> </thead> <tbody> <tr> <td colspan="13">Confidence Factor = 1.00, qd = 1.00, le = 1.00</td> </tr> <tr> <td colspan="13">Press right mouse button and click 'Set Cyclic Shear Resistance Parameters' menu to change Load Case/Combination/Confidence Factor/Displacement Behavior Factor/Importance Factor</td> </tr> <tr> <td></td> <td>361</td> <td>I-end</td> <td>Primary</td> <td>ALL COMBINATION</td> <td>5.2877</td> <td>822.0910</td> <td>cLCB4</td> <td>OK</td> <td>7.4436</td> <td>2628.3800</td> <td>cLCB5</td> <td>OK</td> </tr> <tr> <td></td> <td>361</td> <td>J-end</td> <td>Primary</td> <td>ALL COMBINATION</td> <td>5.2877</td> <td>814.6980</td> <td>cLCB4</td> <td>OK</td> <td>7.4436</td> <td>3195.2900</td> <td>cLCB5</td> <td>OK</td> </tr> <tr> <td></td> <td>365</td> <td>I-end</td> <td>Primary</td> <td>ALL COMBINATION</td> <td>16.3991</td> <td>796.9310</td> <td>cLCB5</td> <td>OK</td> <td>4.4192</td> <td>2537.2200</td> <td>cLCB4</td> <td>OK</td> </tr> <tr> <td></td> <td>365</td> <td>J-end</td> <td>Primary</td> <td>ALL COMBINATION</td> <td>16.3991</td> <td>849.5140</td> <td>cLCB5</td> <td>OK</td> <td>4.4192</td> <td>2695.0400</td> <td>cLCB4</td> <td>OK</td> </tr> </tbody> </table> |   | Elem              | Location        | Seismic Element        | Load        | Cyclic Shear Resistance                       |                                      |   |                         |       |        |  |     | VRy |  |  |  | VRz |  |  |  | Demand (kN) | Capacity (kN) | Load | Remark | Demand (kN) | Capacity (kN) | Load | Remark | Confidence Factor = 1.00, qd = 1.00, le = 1.00 |  |  |  |  |  |  |  |  |  |  |  |  | Press right mouse button and click 'Set Cyclic Shear Resistance Parameters' menu to change Load Case/Combination/Confidence Factor/Displacement Behavior Factor/Importance Factor |  |  |  |  |  |  |  |  |  |  |  |  |  | 361 | I-end | Primary | ALL COMBINATION | 5.2877 | 822.0910 | cLCB4 | OK | 7.4436 | 2628.3800 | cLCB5 | OK |  | 361 | J-end | Primary | ALL COMBINATION | 5.2877 | 814.6980 | cLCB4 | OK | 7.4436 | 3195.2900 | cLCB5 | OK |  | 365 | I-end | Primary | ALL COMBINATION | 16.3991 | 796.9310 | cLCB5 | OK | 4.4192 | 2537.2200 | cLCB4 | OK |  | 365 | J-end | Primary | ALL COMBINATION | 16.3991 | 849.5140 | cLCB5 | OK | 4.4192 | 2695.0400 | cLCB4 | OK | <ul style="list-style-type: none"> <li>EC2 : 2004</li> <li>EC8 : 2004</li> </ul> |
|   | Elem  |   |                   |                 |                        |             | Location                                      | Seismic Element                      | Load  | Cyclic Shear Resistance |       |        |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
|   |   |   |                   |                 |                        |             |   |                                      |   | VRy                     |       |        |  | VRz |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
|   |   | Demand (kN)                                   | Capacity (kN)     | Load            | Remark                 | Demand (kN) |   |                                      |   | Capacity (kN)           | Load  | Remark |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
| Confidence Factor = 1.00, qd = 1.00, le = 1.00  |   |   |                   |                 |                        |             |   |                                      |   |                         |       |        |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
| Press right mouse button and click 'Set Cyclic Shear Resistance Parameters' menu to change Load Case/Combination/Confidence Factor/Displacement Behavior Factor/Importance Factor |   |   |                   |                 |                        |             |   |                                      |   |                         |       |        |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
|   | 361   | I-end   | Primary           | ALL COMBINATION | 5.2877                 | 822.0910    | cLCB4   | OK                                   | 7.4436  | 2628.3800               | cLCB5 | OK     |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
|   | 361   | J-end   | Primary           | ALL COMBINATION | 5.2877                 | 814.6980    | cLCB4   | OK                                   | 7.4436  | 3195.2900               | cLCB5 | OK     |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
|   | 365   | I-end   | Primary           | ALL COMBINATION | 16.3991                | 796.9310    | cLCB5   | OK                                   | 4.4192  | 2537.2200               | cLCB4 | OK     |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |
|   | 365   | J-end   | Primary           | ALL COMBINATION | 16.3991                | 849.5140    | cLCB5   | OK                                   | 4.4192  | 2695.0400               | cLCB4 | OK     |  |     |     |  |  |  |     |  |  |  |             |               |      |        |             |               |      |        |  |  |  |  |  |  |  |  |  |  |  |  |  |   |  |  |  |  |  |  |  |  |  |  |  |  |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |        |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |     |       |         |                 |         |          |       |    |        |           |       |    |  |

ETC.

| Items   | Detail  | Design Code   |
|---|---|---|
| Wall Stiffness Reduction  | <ul style="list-style-type: none"> <li>The wall stiffness scale factor is applied to the wall type in nonlinear analysis like a pushover analysis.</li> </ul>   |   |
| Torsional Amplification Factor Table & Torsional Irregular Checking Table | <ul style="list-style-type: none"> <li>Output the results separately by each direction.</li> <li>Output whether a story diaphragm is applied in the "Note" column.</li> </ul>   |   |
| Calculation of Vcol (column's shear force) in the RC joint design         | <ul style="list-style-type: none"> <li>Change from a column shear by an analysis to the force by the formula below</li> </ul> $V_{col} = [(M_{pr,A}^- + M_{pr,B}^+) + (V_{e2,A} + V_{e1,B}) \frac{h_c}{2}] / \ell_c$  | <ul style="list-style-type: none"> <li>ACI318-19</li> <li>ACI318M-19</li> <li>ACI318-14</li> <li>ACI318M-14</li> <li>NSR-10</li> <li>NSCP 2015</li> <li>NTC-DCEC(2017)</li> <li>KDS 41 20 : 2022</li> </ul> |

ETC.

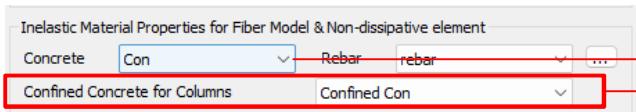
Items

Detail

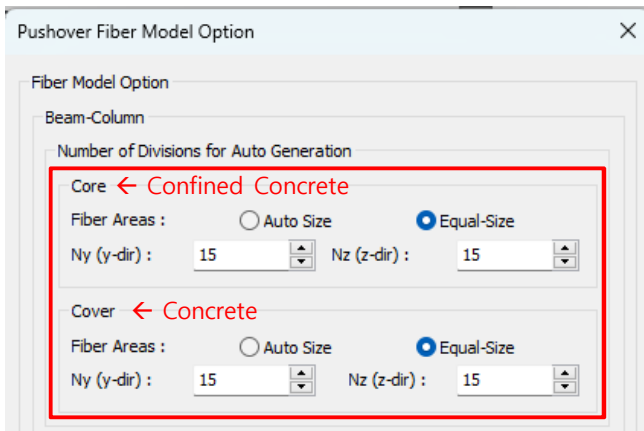
- 'Confined Concrete for columns' is added in the material data dialog box.
- The fiber model of 'Confined' and 'Unconfined' areas are automatically generated based on the hoop bar.

[\[Set the material for 'Confined Concrete' in Material Data\]](#)

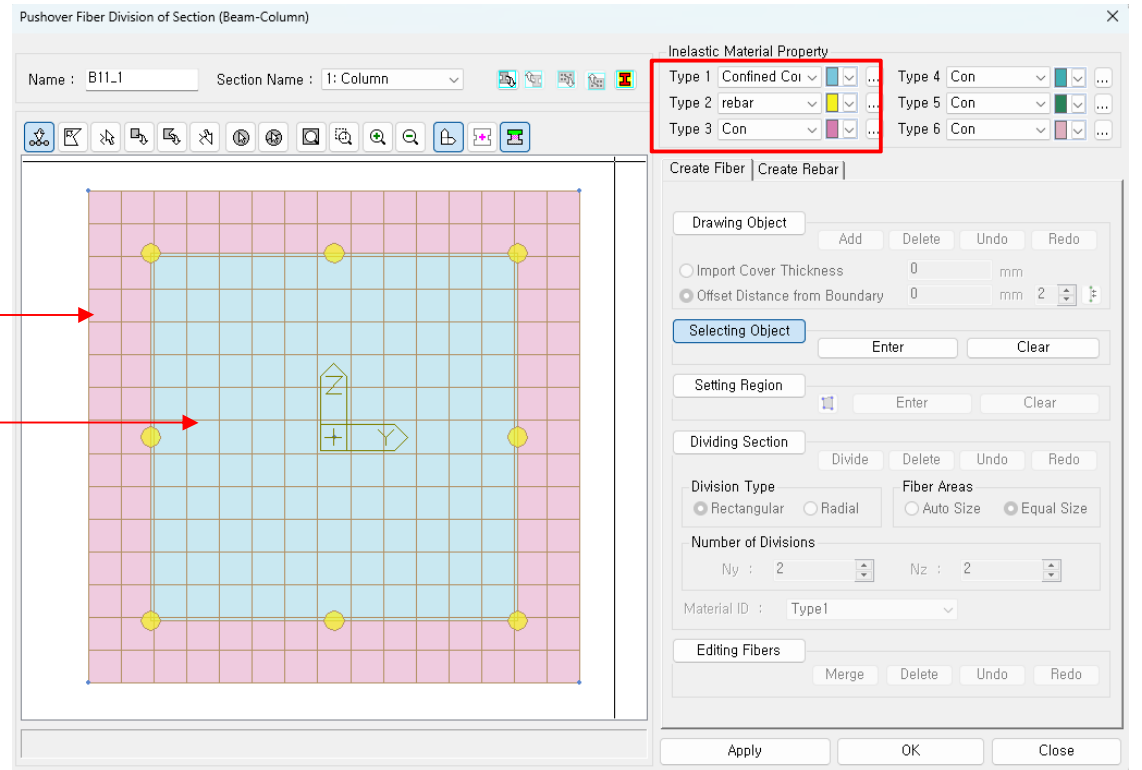
[\[Auto-Generated fiber with Material for 'Confined Concrete'\]](#)



[\[Set the No. of division in Fiber Model Option\]](#)



**\*\* If 'Confined Concrete' is not set, the material of 'Concrete' will be applied to both the core and cover.**



Generation of Column Fiber Model

*Design +*



# Add ACI318(M)-19

- Added ACI318-19 and ACI318M-19.

The screenshot displays the software interface for adding a design code. The 'Design Code' dialog box is open, showing a list of codes. The 'ACI318M-19' and 'ACI318-19' codes are highlighted with red boxes. The main window shows the member properties and a rebar arrangement table.

**Design Code Selection:**

- Design Code: ACI318M-19
- Design Code: ACI318-19

**Member Properties:**

- Member Name: B01
- Material: Concrete 24 MPa
- Main Bar: 400 MPa
- Stirrup: 400 MPa

**Rebar Arrangement Table:**

|                      | END(i)    |                 | Middle    |                 | End(j)    |                 |
|----------------------|-----------|-----------------|-----------|-----------------|-----------|-----------------|
| Moment, top (kN.m)   | 100.00    | OK(0.363)       | 0.00      | OK(0.000)       | 75.00     | OK(0.272)       |
| Moment, bot (kN.m)   | 0.00      | OK(0.000)       | 85.00     | OK(0.309)       | 0.00      | OK(0.000)       |
| Shear (kN)           | 100.00    | OK(0.443)       | 100.00    | OK(0.443)       | 100.00    | OK(0.443)       |
| Rebar, top           | 3         | - #8 OK(0.711%) | 2         | - #8 OK(0.474%) | 3         | - #8 OK(0.711%) |
| Rebar, bot           | 2         | - #8 OK(0.474%) | 3         | - #8 OK(0.711%) | 2         | - #8 OK(0.474%) |
| Stirrup (mm)         | 2         | - #3 @ 250.00   | 2         | - #3 @ 250.00   | 2         | - #3 @ 250.00   |
| Main Bar Space (mm)  | T:138(OK) |                 | B:138(OK) |                 | T:138(OK) |                 |
| Shear Bar Space (mm) | S:250(OK) |                 | S:250(OK) |                 | S:250(OK) |                 |
| SkinBar Space (mm)   |           |                 |           |                 |           |                 |
| Comment              |           |                 |           |                 |           |                 |

**Report Section: END(I)**

- General Information**
  - (1) Design Code : ACI318M-19
  - (2) Code Unit : N, mm
- Material**
  - (1)  $F'_c$  : 24.00MPa
  - (2)  $F_y$  : 400MPa
  - (3)  $F_{ys}$  : 400MPa
- Section**
  - (1) Section Size : 400 x 600mm (R-Section)
  - (2) Cover : 40.00mm
  - (3) Compression : Not Considered
  - (4) Splicing Limit : 50%

# Improvement of Combined footing design

The screenshot shows the 'Member' dialog box in midas Design+. The 'System' is set to 'RC' and the 'Type' is 'Footing (Combined)'. The 'Node' is '13 14'. The 'Column' tab is selected, and the 'Load Combinations (2) ...' checkbox is checked. The 'Column Information' table is as follows:

| No. | Shape     | Span (m) |
|-----|-----------|----------|
| 1   | Rectangle | 0.00     |
| 2   | Rectangle | 4.00     |

The 'Column Section' is set to 'Rectangle' with dimensions Cx = 700.00 mm and Cy = 400.00 mm. The 'Service Load' is Ps = 9417.08 kN and Msy = 2281.55 kN.m. The 'Factored Load' is Pu = 14410.00 kN and Myy = 2241.56 kN.m. The 'Load Combinations (2) ...' checkbox is checked. The 'Check Soil Capacity' table is as follows:

| Check Items                             | Calculated | Criteria | Ratio                |
|---|------------|----------|----------------------|
| Soil Capacity (kN/m <sup>2</sup> )      | -          | 192      | Tension Soil Bearing |
| Q <sub>u,max</sub> (kN/m <sup>2</sup> ) | -          | -        | -                    |
| Q <sub>u,min</sub> (kN/m <sup>2</sup> ) | -          | -        | -                    |

- For the columns in Gen, the design force by each load combination can be imported as the column force in Design+ (Combined footing).  
→ The moment values of the column are included newly.

- If checking off “load combinations”, the user’s input is allowed.

- Improvements

- “Column” Tab was added.

- Column moment was added.

Load Combinations (Service Load)

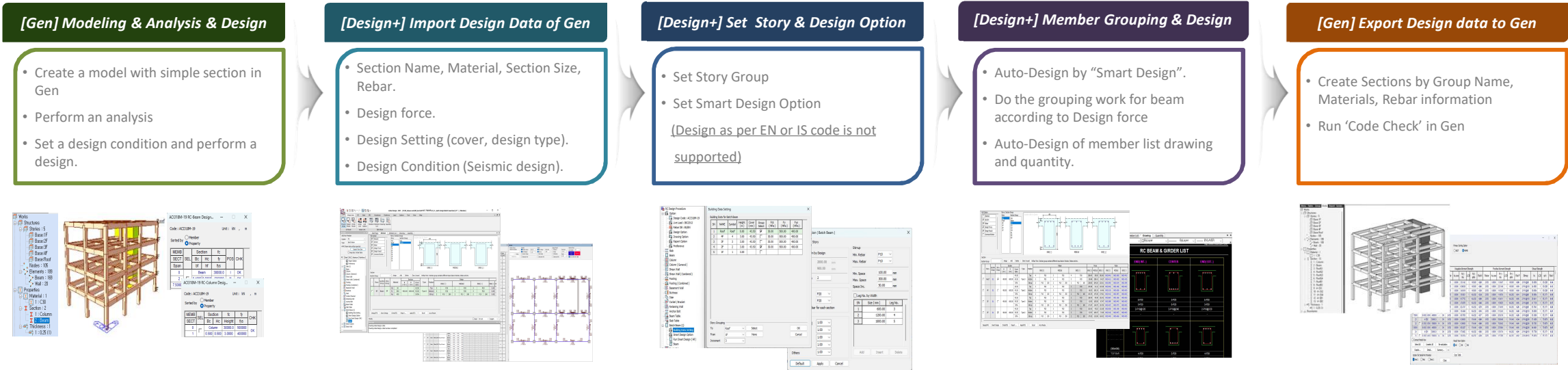
| SN  | CHK                                 | NAME | Ps (kN) | Msy (kN.m) | Description |
|-----|-------------------------------------|------|---------|------------|-------------|
| MAX | <input checked="" type="checkbox"/> | 1s   | 9417.0  | 2281.55    |             |
| 1   | <input checked="" type="checkbox"/> | 1s   | 9417.0  | 2281.55    |             |
| 2   | <input checked="" type="checkbox"/> | 2s   | 555.4   | 2441.50    |             |

Load Combinations

| SN  | CHK                                 | NAME | Pu (kN) | Myy (kN.m) | Description |
|-----|-------------------------------------|------|---------|------------|-------------|
| MAX | <input checked="" type="checkbox"/> | 1    | 14410.0 | 2241.56    |             |
| 1   | <input checked="" type="checkbox"/> | 1    | 14410.0 | 2241.56    |             |
| 2   | <input checked="" type="checkbox"/> | 2    | 1117.5  | 2481.49    |             |

# Batch Beam & Column (New)

- There are many inconveniences when performing design in Gen. For example, when a section needs to be added when grouping members or when the cross section needs to be increased according to design results, analysis and design should be performed again. Since these cases must be performed repeatedly, a lot of time and effort are required depending on the magnitude of the building.
- Batch Design is a design feature to provide convenience for these repetitive parts in Gen, and the procedure is as follows.



- The purpose of Batch Design is to quickly create and link the material, cross-section, and rebar information to Gen for analysis and design in Gen. Please use this product with the understanding that design results may differ slightly due to internal differences in design settings for Gen and Design+.
- Design as per EN or IS code is not supported.

❖ **Manual & Tutorial : [\[Download\]](#)**